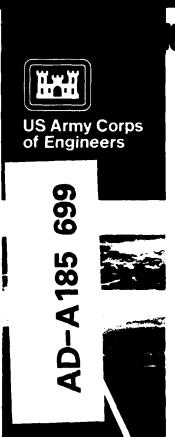
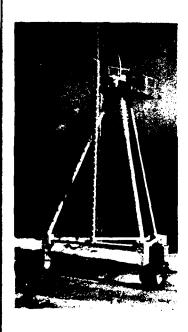


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BEACH AND NEARSHORE SURVEY DATA: 1981-1984 CERC FIELD RESEARCH FACILITY

by

Peter A. Howd, William A. Birkemeier

Coastal Engineering Research Center

DEPARTMENT OF THE ARMY Waterways Experiment Station, Corps of Engineers PO Box 631, Vicksburg, Mississippi 39180-0631





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PREFACE

This report was prepared at the Coastal Engineering Research Center (CERC) of the US Army Engineer Waterways Experiment Station (WES) as part of the Storm Erosion Studies Work Unit, Shore Protection and Restoration Program; Coastal Engineering Area, Civil Works Research and Development. Technical Monitors were Mr. John H. Lockhart, Jr., and Mr. John G. Housley, Headquarters, US Army Corps of Engineers.

Mr. Peter A. Howd and Mr. William A. Birkemeier of CERC's Field Research Facility Group prepared the report under the supervision of Mr. Curt Mason, former Chief, Field Research Facility; Mr. Thomas W. Richardson, Chief, Engineering Development Division; and Mr. Charles C. Calhoun, Jr., and Dr. James R. Houston, Assistant Chief and Chief, CERC, respectively. Messrs. Eugene W. Bichner, Charles R. Townsend III, Michael W. Leffler, Francis E. Sargent, and Ms. Rebecca J. Savage, plus many others, contributed to the collection of the data. Ms. Harriet M. Klein assisted greatly by untangling complexities of the English language. The wave and water-level data presented in the report were collected by CERC's Field Research Facility Measurements and Analysis Work Unit under the direction of Mr. Herman C. Miller. This report was edited by Ms. Jamie Leach of the WES Information Technology Laboratory.

Commander and Director of WES upon publication of this report was COL Dwayne G. Lee. Technical Director was Dr. Robert W. Whalin.

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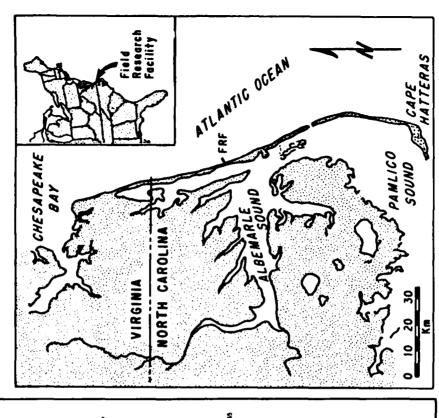
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	Bathymetric map of study area showing locations of the four profile lines

BEACH AND NEARSHORE SURVEY DATA: 1981-1984 CERC FIELD RESEARCH FACILITY

PART I: INTRODUCTION

- 1. The Field Research Facility (FRF) of the US Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center (CERC), was established to provide a research and development capability for field studies of coastal processes. An important part of the FRF operation has been the collection of long-term data sets of waves, currents, tides, atmospheric conditions, and beach profile change. The purpose of this report is to present the first 4 years of highly accurate profile data collected under the Storm Erosion Studies work unit.
- 2. This continuing data set is unique in the field of beach profile studies because of its accuracy, temporal coverage, and concomitant wave, weather, and water-level information. Surveys of four shore-normal profile lines were completed at approximately 2-week intervals. Nowhere else does such a data set exist. It provides a unique opportunity to examine natural profile changes and to test and evaluate models of beach profile response to changing wave, current, and atmospheric conditions.
- 3. The FRF is located just north of the village of Duck, N. C., on the Outer Banks (Figure 1). The facility includes a 561-m-long research pier and support buildings. The beach adjacent to the study area is interrupted only by open pile piers from Cape Henry, Va., to Oregon Inlet, N. C., a distance of 110 km. General information regarding the FRF and the surrounding area is provided in Birkemeier et al. (1985). A comprehensive network of weather and ocean sensors provides continuous monitoring of atmospheric and oceanographic conditions. These data are published in a series of annual (Miller 1984; Miller et al. 1985, 1986) and monthly data reports.
- 4. The data in this report were collected along the four profile lines shown in Figure 2 (Lines 58, 62, 188, and 190). A profile line is defined as a fixed transect across the beach and nearshore which is repetitively surveyed. Table 1 summarizes the location of these lines and the data contained in this report. Based on regular monthly surveys of the bathymetry



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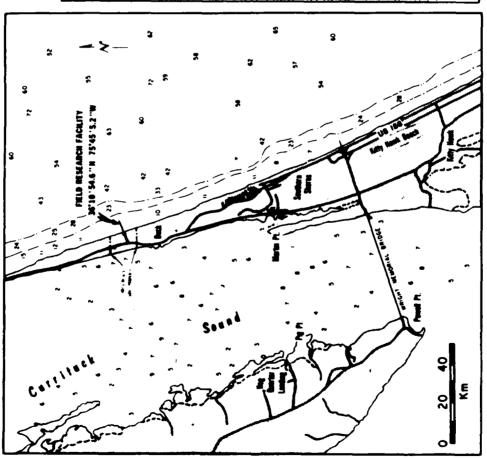
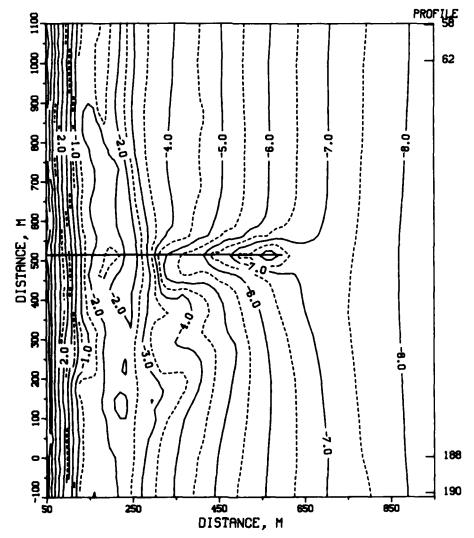


Figure 1. Location of the FRF

Table 1
Summary of Profile Line Data

Profile	Distance Along FRF Baseline	Distance From FRF Pier	First	Last	Number of
Line	m	m	Survey	Survey	Surveys
58	1097.31	580.64	17 Jul 81	13 Dec 84	
62	1005.84	489.21	26 Jan 81	13 Dec 84	119
188	0.00	-516.63	20 Jan 81	17 Dec 84	127
190	-91.40	-608.07	17 Jul 81	17 Dec 84	99

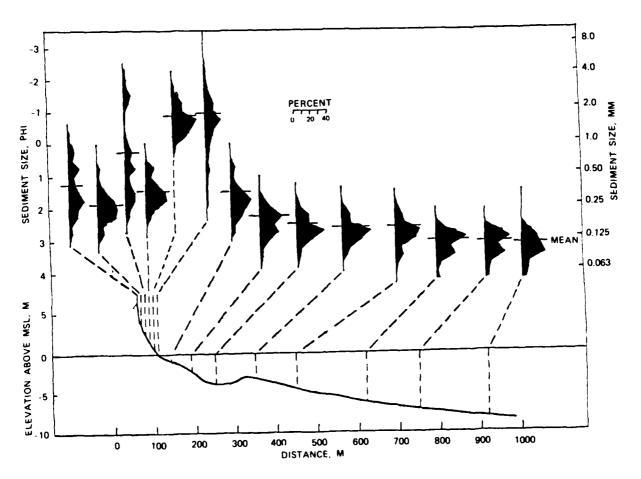


FRF BATHYMETRY 27 NOV 84 contours in meters

Figure 2. Bathymetric map of the study area showing locations of the four profile lines

surrounding the FRF, these lines are located in a region of shore-parallel contours and are sufficiently removed from known pier effects (Miller, Birkemeier, and DeWall 1983).

- 5. The beach is composed of a mixture of quartz sand and carbonate shell debris. The carbonate component may be as high as 20 percent. Mean grain size is greatest on the foreshore where it approaches 1 mm, decreasing offshore to 0.1 mm. Sorting improves in an offshore direction. Figure 3 illustrates the cross-shore variation in sediment size distribution based on a series of samples taken along profile line 188 on 17 March 1982.
- 6. Storm conditions at the FRF are dominated by extratropical northeasters during the winter months and occasionally by tropical hurricanes. During the period of study, a number of significant storms occurred, although no major hurricanes passed the area.



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Figure 3. Distribution of sediment sizes across profile line 188 on 17 March 1981

7. The report includes five parts and six appendices. Part II discusses the survey methods used to collect the profile data and points out the sources of errors and methods used to minimize those errors. Part III presents summary comments about profile characteristics and patterns of profile change as an aid in interpreting the data. Part IV presents the associated wave and water-level data. The report is summarized in Part V. Appendices include plots of all the profiles (Appendix A), tables of the profile data along with a FORTRAN computer program to read and check the data (Appendices B and C), plots of wave height for the 4-year period (Appendix D), tables of wave height and period (Appendix E), and plots of the observed tides (Appendix F).

PART II: PROFILE DATA

- 8. This part describes the methods used to survey the profile data and identifies potential sources of error and how errors were handled. The data for each profile line are a series of distance-elevation pairs measured during a repetitive number of surveys. The data extend from a shore-parallel base-line, located landward of the duneline, out to a usual depth of 8 to 9 m. Elevation data are referenced to the 1929 National Geodetic Vertical Datum (NGVD) using third-order control established at the FRF. Each survey of each profile line is uniquely identified by a profile number and survey number.
- 9. Surveys were initially conducted biweekly, the northern lines one week followed by the southern lines the next. This sequence changed in December 1982 to biweekly surveys of all four lines. Full bathymetric surveys of 15 to 28 lines surrounding the FRF were also conducted monthly. Additional surveys were added to cover significant storms and in support of special experiments. The time interval between surveys varied from 1 to 44 days.

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The CRAB

- 10. The method used to collect the majority of the profile data is described in Birkemeier and Mason (1984). All profiles were surveyed using the FRF Coastal Research Amphibious Buggy (CRAB) shown in Figure 4. Built by the Wilmington District of the US Army Corps of Engineers, this unique three-wheeled vehicle was modeled after a vehicle originally built by Marine Travelift & Engineering of Sturgeon Bay to monitor a Corps of Engineers beach nourishment project.
- 11. The CRAB consists of a tripod of 20.3-cm schedule-80 aluminum tubing, connected at the base by horizontal members 2.1 m above the ground, and an operations platform 10.7 m above the ground. Power is supplied by a 39.5-kW Volkswagen engine on the deck which drives a variable stroke hydraulic pump. This pump transfers hydraulic fluid at $5.5 \times 10^6 \text{ N/m}^2$ or higher to hydraulic motors at each of the wheels. The variable stroke feature of the pump allows an infinitely variable gear ratio in either forward or reverse and constant engine speed. For strength and corrosion resistance, all hydraulic lines are stainless steel except for short flexible sections at the front steering wheel.

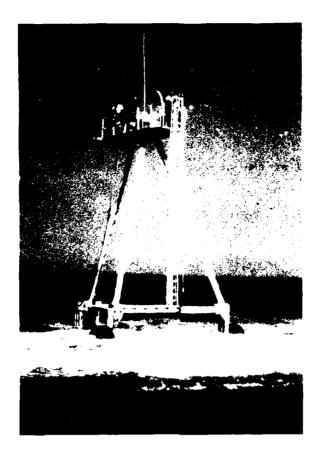


Figure 4. The CRAB

- 12. Total vehicle weight is about 8,200 kg; the distance between the rear wheels is 8.2 m. Though it appears top heavy, the liquid-filled tires and wide wheelbase make it very stable. It has passed a 20-deg tilt test and is designed to withstand even steeper angles.
- 13. Top speed of the CRAB is 3.2 km/hr on land and somewhat less in the water. Since the maximum significant wave height for operation is 2 m, the CRAB is capable of operating in all but the most severe east coast storms. The large tires have a negligible effect on a hard rippled sand bottom; however, scour around the tires has been observed in areas of active wave breaking or strong currents if the CRAB remains motionless. The CRAB cannot be used on soft silty or loose bottoms.
 - 14. All beach and dune surveying was accomplished with the standard

technique of sending a rodperson along the transect, stopping at regular intervals and breaks in slope.

Early Stadia Surveys

- 15. From January to June 1981, the position and elevation of the CRAB were determined using an automatic level, located on the beach, to read a 12.3-m-high stadia board attached to the CRAB. This system was slow and sensitive to a wide range of errors. Primary sources of error included out-of-level or poorly aligned instruments, stadia reading errors, fieldbook and transcription errors, and instrument stationing errors. Estimated accuracy in distance was from ± 0.3 to ± 6 m. Vertical accuracy was estimated to vary from ± 0.03 to ± 0.6 m. Single points or surveys may have been in greater error.
- 16. Errors tended to increase with distance. This resulted from the increased difficulty in reading the stadia board and the greater impact of out-of-level errors. Because of these errors, data collected prior to June 1981 end approximately 600 m offshore. Points farther offshore were of questionable accuracy and have been dropped.
- 17. Although of inferior quality to later surveys, the stadia survey data have been retained in the data set because the configuration of the profile lines (which is accurately represented) during this period is unusual and not later repeated.

Electronic Survey System

18. In order to improve the speed and accuracy of the surveys, a Zeiss Elta-2 electronic surveying instrument with automatic data recording was used after June 1981 (Figure 5). This instrument incorporates in one compact unit a first-order electronic theodolite, distance meter, microprocessor, rechargeable power supply, and interchangeable solid state memory module. When optically aimed at a reflecting prism on the CRAB, the instrument uses a collimated infrared beam to measure the distance and the electronic theodolite to measure both horizontal and vertical angles. The microprocessor then uses these measurements plus the coordinates of the instrument to compute X, Y, and Z Cartesian coordinates of the ground point under the CRAB (corrected for

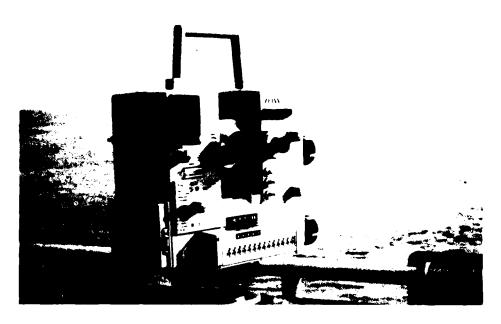


Figure 5. Zeiss Elta-2 electronic surveying instrument

earth curvature).

- 19. The stated operating range is 2 km with a triple prism assembly as used on the CRAB. Working accuracy of ± 3 cm or better is possible in both horizontal and vertical coordinates. Actual accuracy in a repetitive survey program is less because of changing atmospheric conditions, different instrument setups, and differences in the actual points surveyed.
- 20. The high accuracy of the system is shown in Figure 6 (Birkemeier and Mason 1984), which shows 10 repetitive surveys of a profile line collected over a 2-day period under near ideal conditions. While there is movement of the nearshore bar during the period shown, the stability of the offshore zone is of greater interest. Seaward of 220 m, the average range in elevation was 5 cm. The standard deviation of the 10 elevations for a given distance was usually less than 2 cm.
- 21. Only about 10 sec are required to aim, shoot, and record each survey point. Because the actual coordinates of each point are displayed, the CRAB can easily be kept on line to within ± 1.5 m through radio communications between the CRAB driver and the instrument operator.

- 22. Once the survey is complete, the solid state memory is removed from the Zeiss, and the data are transferred through a Zeiss interface to a main-frame, desktop, or minicomputer. Because the system only requires proper aim from the operator, instrument reading errors and fieldbook entry errors are eliminated.
- 23. A unique feature of the Zeiss system is its ability to accept and record an additional piece of information (up to seven digits) with every survey point. This was used to manually enter the angular tilt of the CRAB, which was measured with two orthogonal tilt meters. Up to 14 deg of tilt was recorded on steep portions of the beach. The survey data were adjusted during processing to account for the tilt.

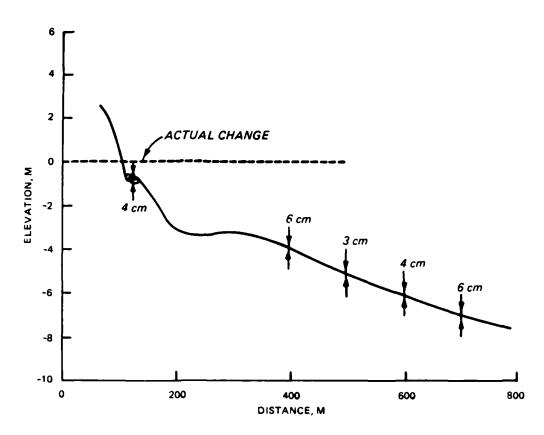
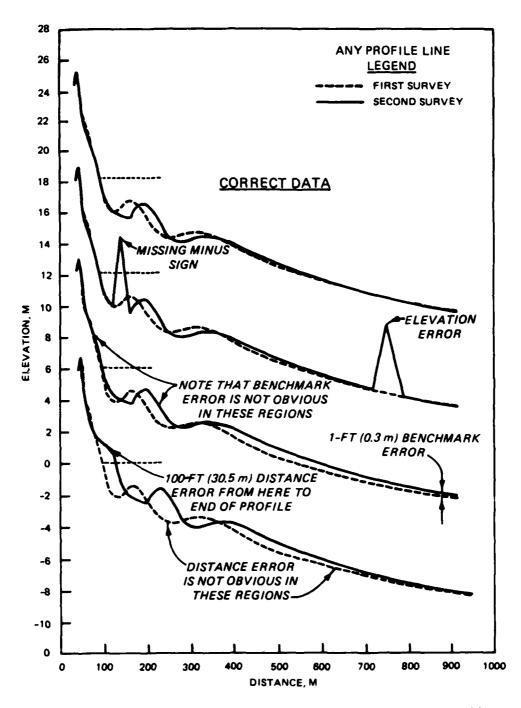


Figure 6. Results of 10 repetitive surveys of a single profile line using the CRAB/Zeiss system

Error Minimization in Profile Data-Collection Methods

Error types

- 24. The biases and errors of the CRAB-Zeiss method can be broken down into two distinct categories: limitations of the instrument and operator errors.
- 25. The Zeiss Elta-2 is capable of measuring both horizontal and vertical angles to ± 0.6 sec of arc and distances to ± 1 cm in the mode most commonly used at the FRF. The specified range when using a triple prism configuration is 2 km. Increasing the number of prisms increases the range.
- 26. The instrument is sensitive to atmospheric and climatic variation since it uses the speed of light to determine distance and optical aiming to measure the angles. The instrument does allow for rough adjustment for these variables. During the summer months, heat shimmer and temperature gradients near the land-sea interface may also affect the accuracy of the angular measurements. These errors are assumed to be negligible relative to other types of errors.
- 27. On one occasion the Elta-2 developed an internal problem which introduced a gradual bias into the data. This bias was identified and removed during processing. Errors of this type are difficult to remove because they occur radially from the instrument's position and do not uniformly affect the data. The instrument was repaired, and the malfunction did not reoccur. Treatment of errors in the data is discussed below.
- 28. Operator errors can result from improper leveling of the instrument, an error in positioning the instrument in coordinate space (particularly in elevation), movement of the tripod during the survey, and mis-aiming the instrument at the proper location on the prism cluster while taking the measurement. Constructed examples of typical nearshore survey errors and their impact are shown in Figure 7. All the measured points are affected by improper leveling or improper location in coordinate space. Individual points are affected by incorrect aim.
- 29. A different type of operator error results when topographically important points, such as the bar crest or trough, are missed. Survey points are selected based on the timed travel of the CRAB. More points are taken close to shore where the profile is more complex. It is possible for the



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Figure 7. Samples of typical surveying errors and their effects

Zeiss operator to follow the vertical movement of the CRAB, but some significant features were probably missed.

- 30. A third type of operator error is caused by the instrument being triggered to begin a reading prior to properly aiming at the prisms. This short cut of triggering, then sighting the point, results in sampling the azimuth and zenith angles at the time of triggering and later use of these incorrect angles with the distance to the prisms to calculate the CRAB location. Errors affecting single points are usually easy to detect and remove.
- 31. An additional but unquantified source of error results from the thermal expansion and contraction of the CRAB frame and its liquid-filled tires. There is also some "error" introduced into the data by averaging the elevation over the 8.2-m base of the CRAB. The prism and the stadia board were mounted in the vertical plane of the back wheels equidistant between them. Some small error also occurs when sediment is compressed by the weight of the CRAB. Divers have observed tread marks on the bottom following the passage of the CRAB. No adjustment to the data has been made to account for these effects. It is suspected that they may be on the order of 3 to 6 cm. This amount of variation combined with the slight uncertainty of the over 100 different instrument setups results in a survey noise level that obscures small bed-level changes along the offshore reaches of the profiles.

Error minimization

32. Two steps were taken to minimize the errors associated with the operation of the Zeiss. First, only known locations were chosen as sites for the setup of the instrument, random locations were not used, and each survey always began with a shot to a prism in a known location. If the measured location of the prism was outside certain tolerances, ± 6 cm horizontal or ± 1.5 cm vertical, the instrument was restationed. Second, periodic checks to the reference prism during the course of the survey helped ensure that the instrument had neither gone out of level nor was in need of restationing.

Error identification

33. Errors in the data are most easily recognized through comparison with the past data collected for that profile. All data were compared with the immediately prior survey of the profile. More often than not, this comparison shows where possible errors occur. The suspect points can then be inspected more carefully and a decision made as to whether the point or points were in error or represented real changes on the profile. Figure 7 shows the

utility of comparison. Questionable data, where no clear error could be discerned, were noted and compared with the next survey as well. This provides a double check. Errors were also identified using the measured location of the reference prism shot in during the stationing procedures. Use of these measurements will be discussed in the next section.

Error correction

- 34. Corrections made to the data consist of two primary types; deletion of points, and addition or subtraction of biases. The biases were either constant because of improper stationing of the instrument or gradual (distance dependent) resulting from improper leveling of the instrument. Vertical errors from mis-leveling become increasingly evident with increasing distance. Vertical corrections to the data were made employing the known elevation of the reference prism and by comparison with surveys of the same profile immediately before and after the questionable data.
- 35. Most often the constant vertical offsets were the result of either improper stationing of the instrument (setting its elevation incorrectly), or, rarely, improper entry of the elevation of the prism cluster on the CRAB. Both of these errors could be traced to the data through the recorded setup procedure. If there was no evidence of a mistake in stationing the Zeiss or entry of the prism height, removal of the suspected bias was dependent on two factors; the bias had to extend over the entire profile (past the normal closure point), and there had to be no reason to expect evidence of profile activity at depth. For instance, if the measured profile showed significant erosion at a depth below the extreme profile closure depth during a period of below-normal wave activity, errors were strongly suspected. However, the bias was removed from the data only after a second survey of the profile further indicated that an error had been made.

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- 36. Gradual biases, or rotations of the data, which result from calibration or leveling errors rather than stationing errors, can be more difficult to discern in the data. These corrections were made only to the early level and stadia board data. The shift in the data could be directly attributed to a miscalibration of the automatic level, or to a leveling error during or after setup of the instrument. The rotation needed to correct the data was determined by recalibration of the level.
- 37. Another category of data editing was the removal and/or correction of obviously erroneous data points. These points were usually the result of

improper entry of the height of the CRAB prism cluster into the Zeiss, errors due to the incorrect targeting of the prism cluster, or points which were unaccountably, but obviously, wrong.

- 38. The data were also corrected for the angle of tilt of the CRAB. The CRAB operator measures the two orthogonal angles on the main axes of the CRAB. Angles greater than 4 deg are radioed to the Zeiss operator who enters them into the recorded data. The angles are automatically accounted for during processing of the data.
- 39. Corrections made to the data, (except CRAB tilt corrections), are recorded in processing and data-collection logbooks and are coded into the data file. The meaning and format of the codes are presented in Appendix B.

Special Notes on the Survey Data

- 40. A number of surveys within the data set require specific discussion regarding data quality. The early stadia surveys (January to 1 June 1981) have already been described. From approximately 14 December 1982 until 9 February 1983, the Zeiss Elta-2 was intermittently producing questionable results which appeared as a systematic vertical error. From 24 February 1983 through 28 March 1983, the instrument was being repaired and alternate methods were employed. These included the use of the stadia board and automatic level to determine elevation and a Motorola Mini-Ranger positioning system to determine offshore distance (24 February to 3 March). A loaner Zeiss instrument was also employed (22 March to 28 March).
- 41. Because this was an unusually active period of profile response with a number of significant storms occurring, the data during this period have been retained in the data set. They do accurately reflect the changes in profile configuration which occurred, but the horizontal and vertical accuracies are less than for the remaining CRAB/Zeiss data.
- 42. Data prior to December 1981 were saved only to whole feet in distance and tenths-of-a-foot in elevation (normal accuracy for beach profile data). Because of the greater accuracy of the CRAB/Zeiss data, subsequent data are stored to tenths-of-a-foot in distance and hundredths-of-a-foot in elevation. This too has an impact on the overall accuracy of the data.

PART III: PROFILE RESULTS

- 43. The data presented in this report have been described by Birkemeier (1985a). Some of the discussion from that report is repeated here as an aid in interpreting the data. Profile changes at the FRF occur at time scales ranging from minutes to annual cycles and longer. Time scales resolvable with the data in this report vary between a few days and 1 to 2 years. Though the profiles have varied in configuration from nearly unbarred to triple barred, they typically exhibit a double bar with a narrow and well-defined inner bar and a broad outer bar. Figure 8 illustrates five of the configurations observed during the study.
- 44. The profile envelope defined by all surveys of line 188 is shown in Figure 9. The plot of maximum vertical change in the upper half of Figure 9 indicates most profile activity is restricted to depths less than 7 m with little measurable vertical variation at deeper depths (only 15-cm maximum variation at 8-m depth). It is not clear how much of this 15 cm is real. Birkemeier (1985b) examined the changes within the data set caused by storms and found that significant storm-induced bed-level changes (>3 cm) occurred at depths less than -6.4 m relative to mean low water (-6.8 m below National Geodetic Vertical Datum, NGVD).

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- 45. One of the best indicators of profile configuration and activity is the location of the bar crest. Large changes to the profile in terms of volume changes always result in movement of the bar system. Minor storms typically force only the inner bar offshore, while larger storms may move both bars offshore, depositing sand in deeper water. Storm changes were rapid, occurring over periods of 1 to 5 days. The rapidity of these changes is discussed further in Sallenger, Holman, and Birkemeier (1985).
- 46. Onshore bar movement usually corresponded to periods of low waves between storms. The speed and the amount of recovery were affected by the wave conditions and by the poststorm configuration of the profiles. All the bar features tended to disappear during extended periods of low wave conditions.
- 47. An example of the modifications caused by storms is shown in Figure 10. The surveys bracket a series of three storms with the most severe occurring 13-15 November 1981. In contrast, the slow recovery from the changes caused by the fall 1981 storms occurred during 6 months of relatively

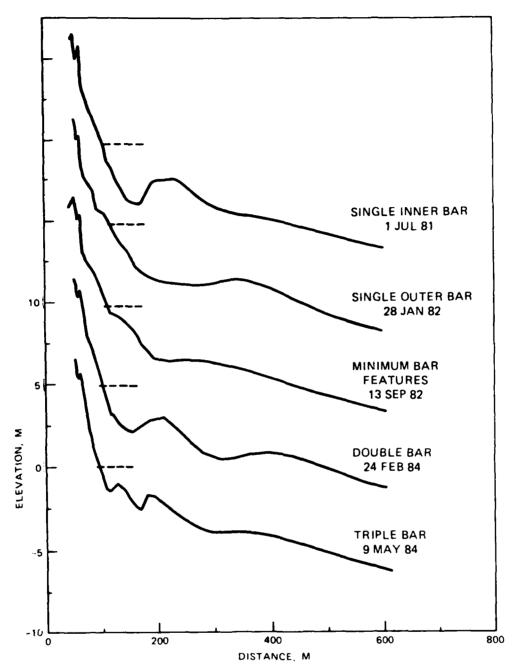
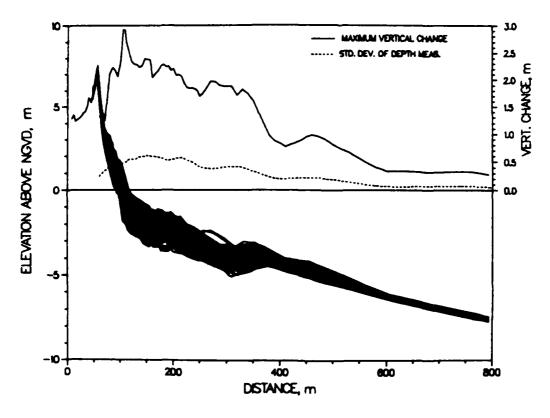


Figure 8. Typical profile configurations occuring in the data set for profile line 62

calm conditions from February to August 1982 (Figure 11).

48. A critical feature of this data set is the fact that four profiles separated in space were measured. Thus, some feeling for the three-dimensional response of the beach is possible. Users of these data are



PROFILE LINE 188, 127 SURVEYS FROM 20 JAN 81 TO 17 DEC 84

Figure 9. Envelope of all surveys of profile line 188

referred to Sallenger, Holman, and Birkemeier (1985) and Howd and Birkemeier (1987) for a discussion of the rapid three-dimensional changes that have been observed at the FRF. As an example, Figure 12 shows profiles 58 and 62 for a sequence of days during October 1982. Initially, both profiles show the bar moving offshore. By the 15th, the bar has begun to migrate onshore at line 62, but continues to move offshore along line 58. (These two profile lines are separated by less than 100 m.)

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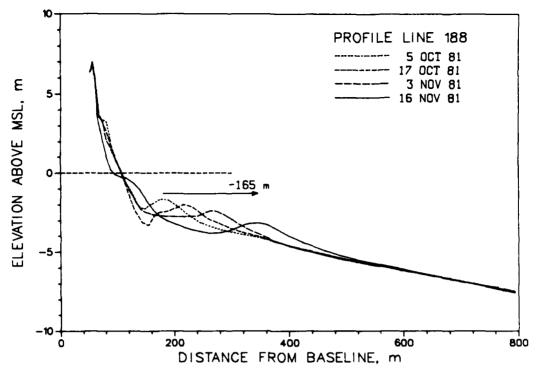


Figure 10. Rapid offshore movement of sediment at line 188 resulting from passage of three fall 1981 storms

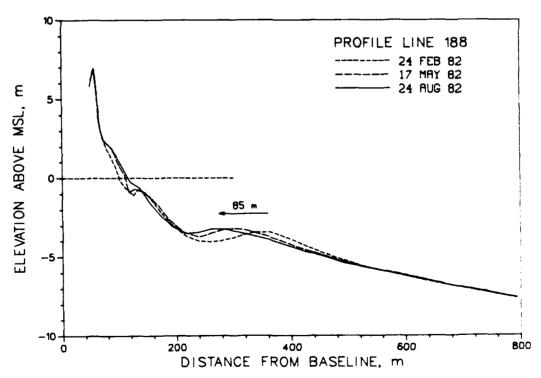
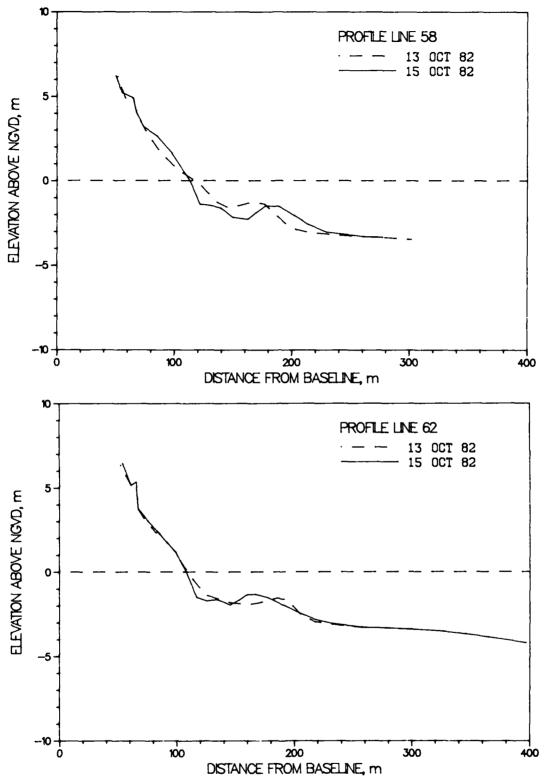


Figure 11. Slow onshore recovery of the outer bar during a 6-month period of low wave conditions



THE PROPERTY SECTION OF STREET STREET,
Figure 12. Evidence of three-dimensional profile response at lines 58 and 62 during October 1982

PART IV: WAVE AND WATER-LEVEL DATA

Wave Height and Period

- 49. The wave heights plotted in Appendix D and tabularized in Appendix E were collected as part of the routine collection program of the FRF Measurements and Analysis work unit. Details of the collection of this data are available in the FRF Annual Data Summaries (Miller 1984; Miller et al. 1985, 1986). The data from a number of gages are sampled at 4 Hz, every 6 hr (hourly during storms) for 20 min. The energy-based significant wave height H_{m0} is computed as four times the standard deviation of the 20-min record. The wave period is computed as period associated with the peak of the wave spectra.
- 50. To provide as complete a record as possible, data from two gages have been combined. The majority of the record is from Gage 625, a Baylor wave staff gage located at the seaward end of the pier. When this gage was inoperative, data from Gage 620, a Waverider buoy located directly off the pier end in 18 m of water, were transformed to the pier end location using the the method of Hallermeier (1983). This method considers frictional dissipation and was developed using data from the FRF.
- 51. During large storms, Gage 625 was in the surf zone and wave heights were saturated, i.e., limited by wave breaking. The maximum wave height limit depends on water level but is usually under 3 m. The maximum recorded wave height of 3.5 m occurred during a storm in November 1981 that coincided with abnormally high spring tides.
- 52. The tables in Appendix E contain daily measurements of wave height and period for wave heights under 2 m and measurements every 6 hr for waves over 2 m.
- 53. More detailed wave information, including wave spectra and data from other gages, is available through the CERC Coastal Engineering Information and Analysis Center (CEIAC).

Water-Level Data

54. The water-level data presented in Appendix F were measured at a National Oceanic and Atmospheric Administration/National Ocean Service (NOAA/NOS) tide station located at the end of the research pier. The data are recorded every 6 min. NOS interpolates missing values using data from nearby gages, accounting for known time lags and elevation differences. The data presented in Appendix F represent the total water-level variation including both the astronomical tides and storm surges. The storm surge is usually defined as the difference between the actual water level and the predicted tides. The total water level should give a better indication of possible forcing of profile change than would the predicted tides or storm surge alone.

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55. Because of the voluminous amount of water-level data, Appendix F includes only plots of the water level. More detailed data are available through CEIAC or from NOAA/NOS.

PART V: SUMMARY

- 56. Four years of high-quality beach profile data collected at the FRF are presented. These data are unique in that they cover the most active part of the profile from the dune out past the depth of closure. The data offer a rare look at the dynamic and often surprising changes that naturally occur in the nearshore zone. The majority of the profile data were collected using the FRF CRAB and a highly accurate electronic surveying instrument. Some relevant dynamic parameters to profile change (wave height, period, and observed tides) are also presented.
- 57. The data should be useful to coastal engineers and researchers who need to have an understanding of the dynamic nature of the nearshore zone. They can provide input and calibration data to numerical and physical models of profile changes. Long-term and seasonal profile envelopes can be computed and used as a guide for determining cable and ocean outfall burial depths and where best to place wave- and current-measuring instruments.

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APPENDIX A: SURVEY PLOTS, 1981-1984

This appendix contains plots of the survey data included in Appendix B. The plots are presented by profile number, starting from the north end of the Field Research Facility property. Refer to Figure 1 of the main text for the location of the profile lines with respect to the pier. Each profile is plotted along with the preceding profile; thus, the change between surveys can be seen. The most recent survey is shown as a solid curve; the previous survey is dashed. The dates of the surveys are given to the right of the data; the lower date corresponds to the solid line.

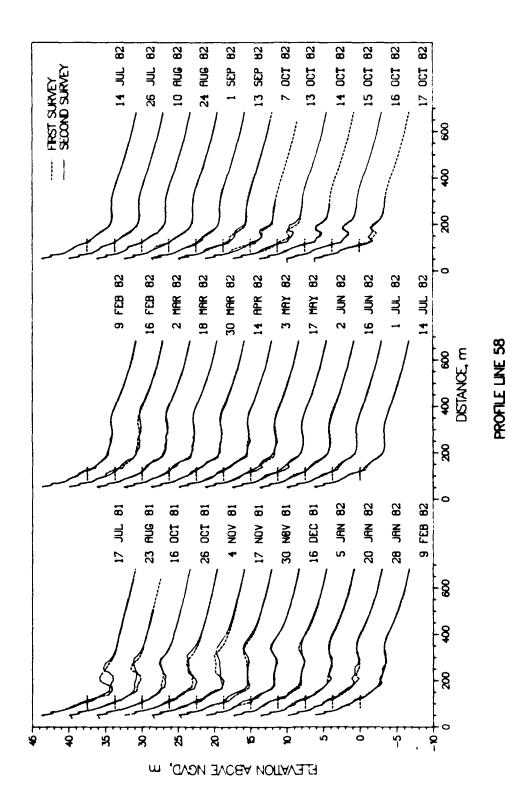
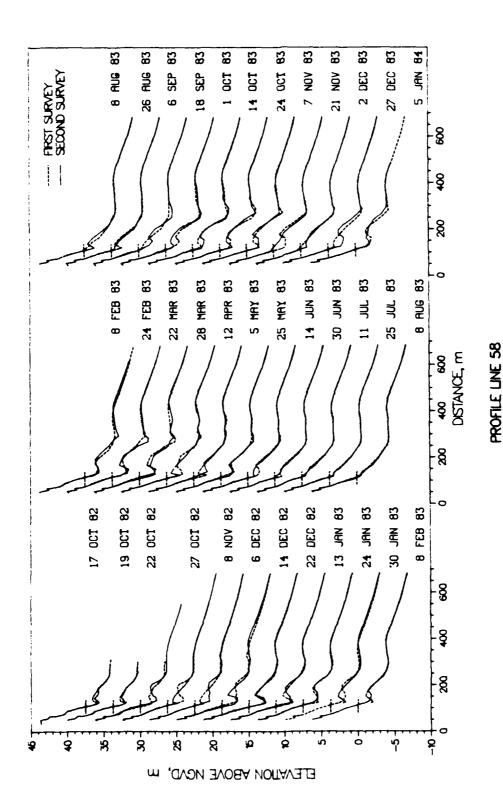


Figure Al. Profile line 58, 17 Jul 1981 - 17 Oct 1982



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Figure A2. Profile line 58, 17 Oct 1982 - 5 Jan 1984

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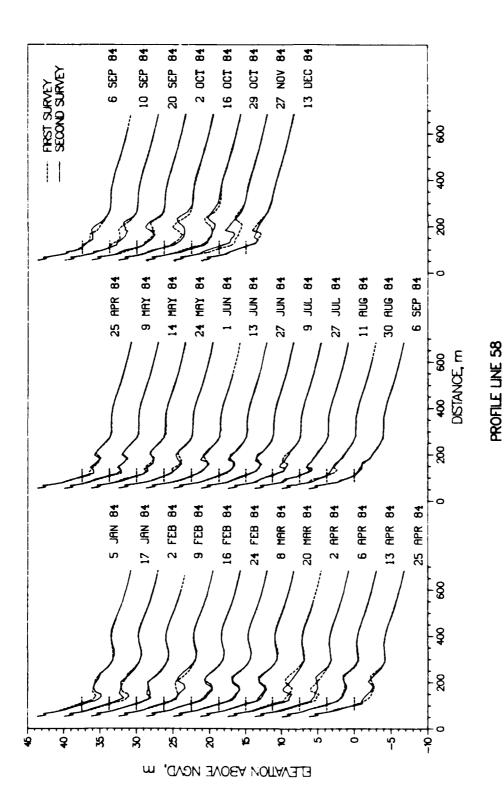
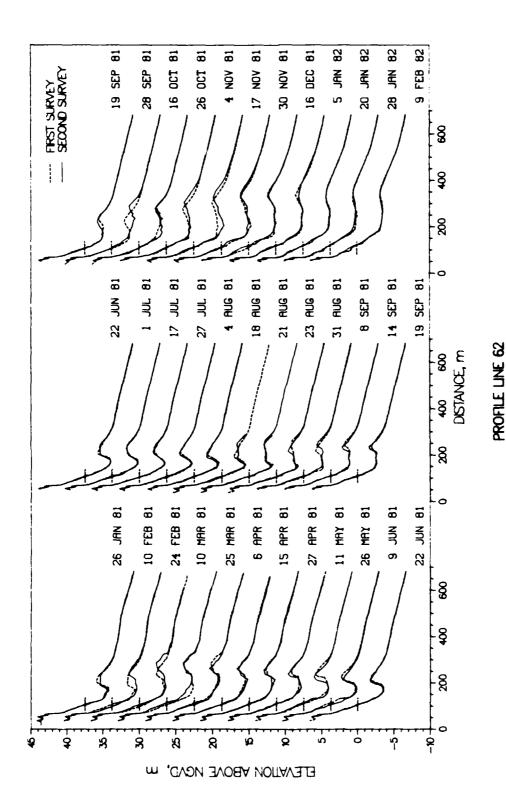


Figure A3. Profile line 58, 5 Jan 1984 - 13 Dec 1984



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Figure A4. Profile line 62, 26 Jan 1981 - 9 Feb 1982

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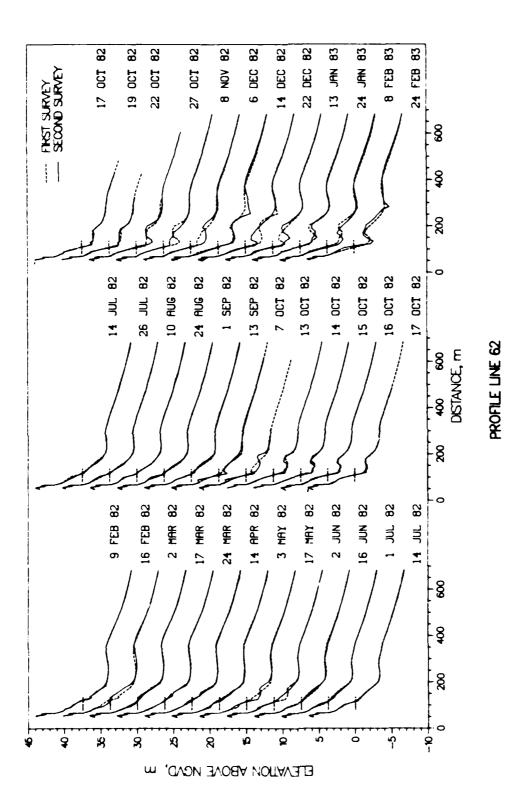
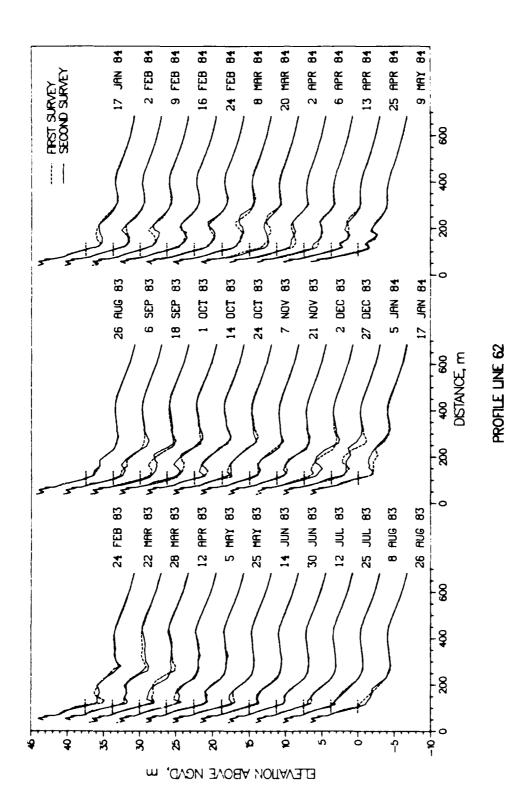


Figure A5. Profile line 62, 9 Feb 1982 - 24 Feb 1983



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Figure A6. Profile line 62, 24 Feb 1983 - 9 May 1984

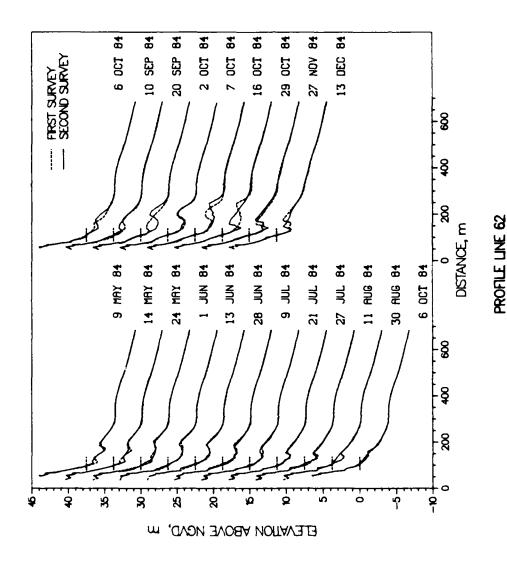
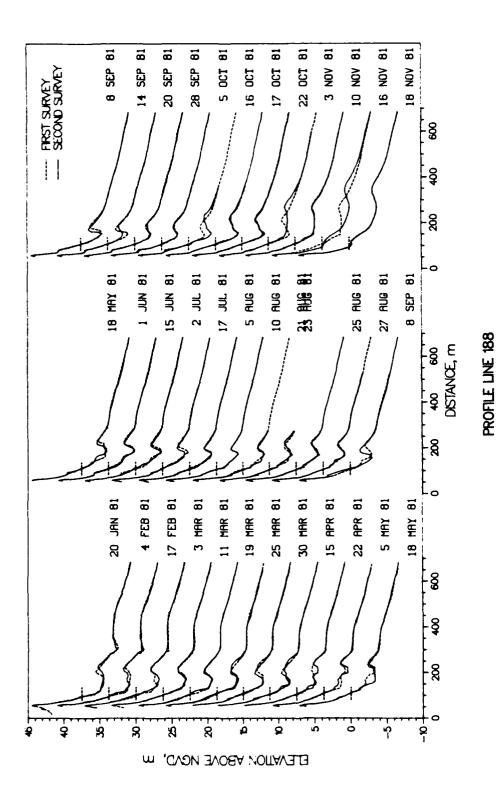


Figure A7. Profile line 62, 9 May 1984 - 13 Dec 1984



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Figure A8. Profile line 188, 20 Jan 1981 - 18 Nov 1981

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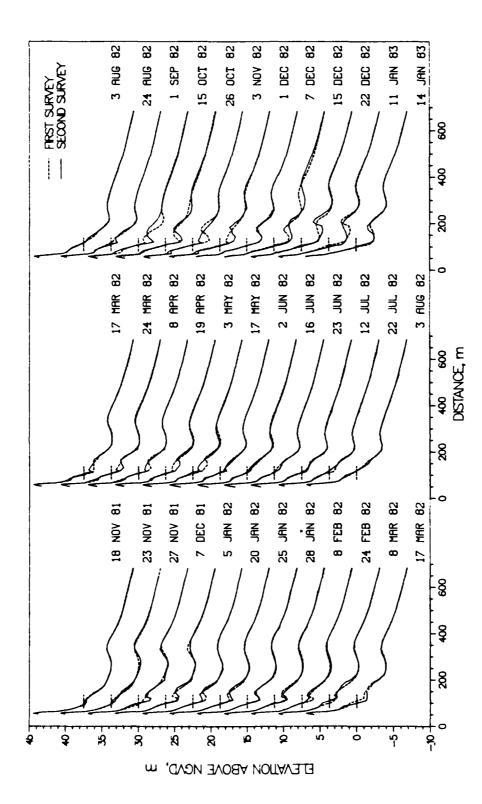
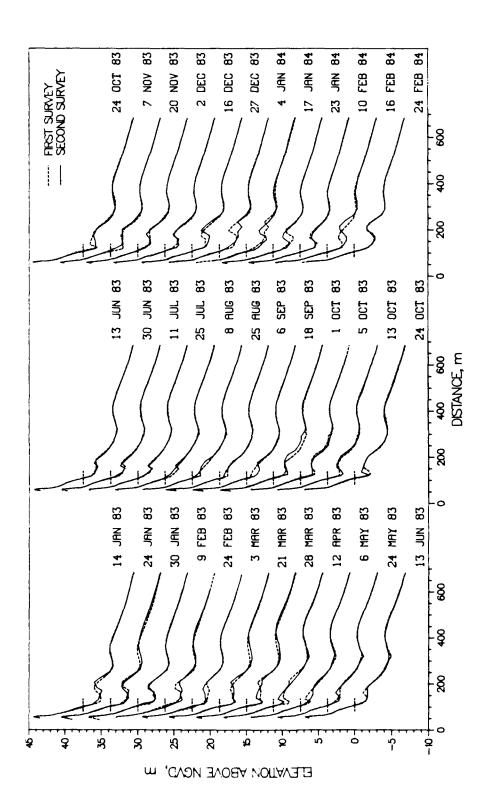


Figure A9. Profile line 188, 18 Nov 1981 - 14 Jan 1983

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Figure AlO. Profile line 188, 14 Jan 1983 - 24 Feb 1984

PROFILE LINE 188

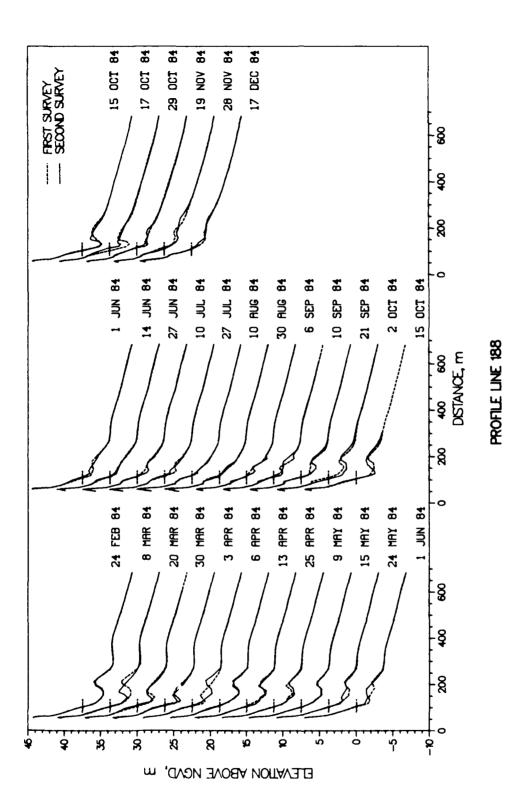
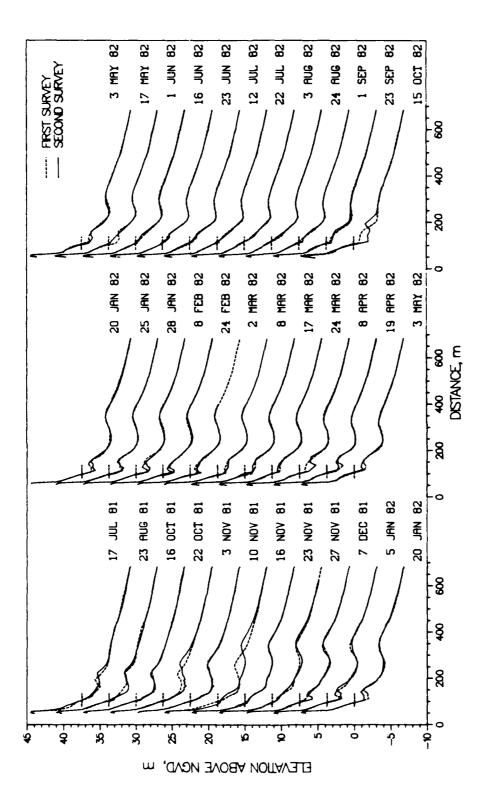


Figure All. Profile line 188, 24 Feb 1984 - 17 Dec 1984

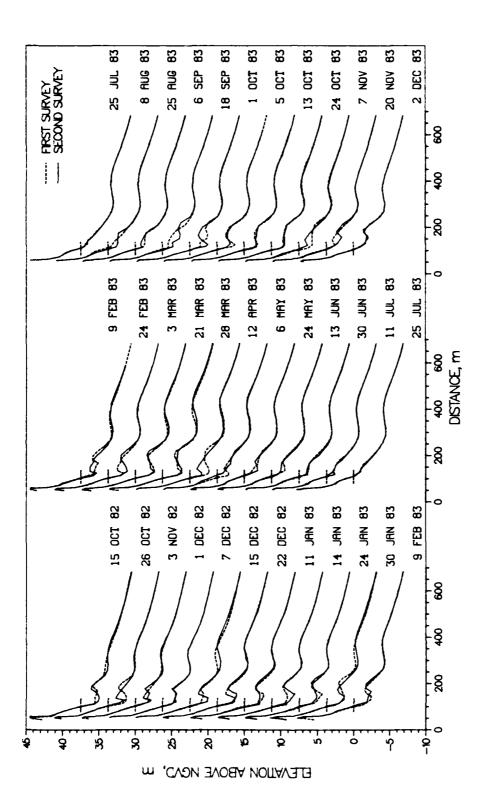


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Figure A12. Profile line 190, 17 Jul 1981 - 15 Oct 1982

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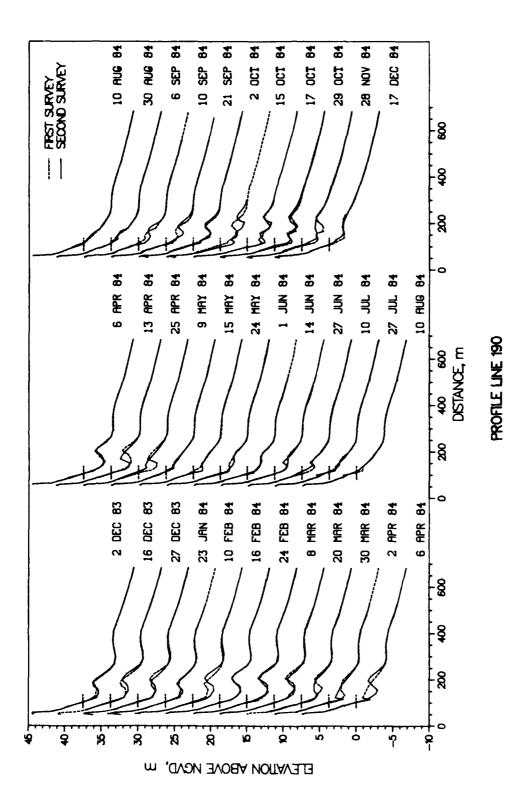


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Figure A13. Profile line 190, 15 Oct 1982 - 2 Dec 1983

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Figure A14. Profile line 190, 2 Dec 1983 - 17 Dec 1984

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APPENDIX B: SURVEY DATA LISTING

- 1. This appendix contains the profile data in BPAS Edit 2 card format (Flemin; and DeWall 1982),* along with a checksum value. When entering the data into a computer, do not enter any values past column 80. These are produced when the data are run through the program given in Appendix C. Use the given values to check your version for possible data-entry errors.
 - 2. The format of the data is as follows:

First card in each record

Position	Entry description	Format
1-2	Locality Code (ILOC)	A2
3-5	Profile line number (IPROF)	13
6-9	Survey identification number (ISUR)	14
10	Card number (always 1 for first card) (N)	A1
11-16	Date of survey (IDATE)	16
17-21	Time of survey (ITIME)	15
22-24	Number of coordinate pairs for survey (I)	13
25-29	Minimum elevation for survey (MIN)	F5.2
30-40	Data change codes (INFO)	A11
41-80	First four distance-elevation pairs (Y,Z)	4(F5.1,F5.2)

Continuation Cards

1-9	Same as for first card	
10	Card number (2-9, then A-Z)	A1
11-80	Seven distance-elevation pairs	7(F5.1.F5.2)

If there are exactly four coordinate pairs (only one card needed), there must be a second blank card following.

3. The format statement to read the data is as follows:

```
READ (??,????) ILOC, IPROF, ISUR, N, IDATE, ITIME, I, MIN, .INFO, (Y(J), Z(J), J=1,I)

7777 FORMAT (A2,I3,I4,A1,I6,I5,I3,F5.2,A11,4(F5.1,F5.2),/,(10X, .7(F5.1,F5.2)))
```

4. The correction codes contained in the INFO field have the following meanings:

G = Gradual correction	<pre>C = Constant correction</pre>
H = Horizontal correction	V = Vertical correction
O = Deletion of points	A = Addition of points
E = Entire profile	S = Selected random points
O = Offshore points	B = Beach points
MR = Mini-Ranger data	

^{*} See References at the end of the main text.

The remaining space is used to give an indication of the magnitude of the changes made, either by the inclusion of the number of points affected or by the magnitude of the change, or both.

5. The survey data are shown in Table B1.

Table Bi
Survey Data for Lines 58, 62, 188, and 190 for 1981-1984

39 58	291810717 1200 50-3200 1550 1980 1680 2050 1830 1690 1940 1540	56
39 58	292 2100 1530 2220 1340 2450 1040 2620 930 2750 800 2900 710 3080 590	0
39 58	293 3350 340 3390 370 3790 0 4090 -300 4390 -620 4620 -980 4890-1000	13
39 58	294 5050-1100 5240-1100 5720-1110 6090 -830 6430 -610 6830 -540 7260 -580	75
39 58	295 8190 -810 9040 -990 9670-112010510-125011700-135012740-141013880-1490	45
39 58	29615040-158016240-167017610-179019270-192021260-208022410-217023870-2260	15
39 58	29725670-239027100-247028460-254030200-265031490-273032950-280034210-2900	18
39 58	29835390-295036600-301037870-306039340-3200	31
39 58	371810823 1600 43-2080 1690 2050 1810 1720 1940 1550 2140 1640	16
39 58	372 2240 1330 2400 1130 2490 1000 2840 630 3280 310 3620 -10 3820 -270	46 315
39 58	373 4080 -380 4310 -500 4660 -680 4900 -850 5130 -980 5440-1000 5680-1010	6
39 58	374 5910-1020 6080-1060 6360-1090 6630-1160 6980-1150 7260-1150 7510-1030	37
39 58	375 7750 -990 7970 -790 8330 -710 9080 -820 9610-104010030-113010460-1200	68
39 58	37611060-128011830-134012630-140013410-148014180-153015120-160016090-1670	42
39 58	37716840-175017900-184019320-194021000-2080	73
39 58	461811016 1600 39-1760 1240 1910 1240 1940 1500 1960 1690 2020	99
39 58	462 1870 1620 2070 1560 2080 1590 2200 1410 2710 730 2820 620 3140 330	67
39 58	463 3400 90 3750 -150 4010 -360 4400 -540 4870 -760 5210 -850 5660 -890	26
39 58	464 5970 -870 6340 -900 6340 -900 6690 -940 7180 -970 7680 -970 8060 -930	54
39 58	465 8390 -900 8760 -860 9030 -830 9440 -830 9760 -86010110-101010390-1080	88 560
39 58	46610790-118011610-131012630-143013450-148014270-156014890-162016570-1760	13
39 58	491811026 1400 45-2380 1700 2030 1910 1580 2150 1570 2320 1200	52
39 58	492 2520 920 2770 670 2850 620 3020 460 3310 210 3570 20 3870 -280	9
39 58	493 4110 -380 4470 -530 4780 -680 5090 -760 5430 -850 5670-1020 5920-1020	88
39 58	494 6150-1060 6500-1070 6760-1030 7010-1070 7310-1080 7660 -960 7880 -960	36
39 58	495 8200 -900 8530 -860 8950 -790 9400 -810 9820 -92010490-110011210-1230	40
39 58	49612020-136012730-143013420-14901444C-157015450-167016570-176017550-1850	56
39 58	49718920-195020130-203021530-212022830-223023990-230025650-2380	99
39 58	501811104 1545 43-2920 1700 2010 1920 1570 2180 1460 2460 990	28
39 58	502 2680 740 2820 590 3060 420 3520 200 3900 -100 4040 -290 4420 -410	13 434
39 58	503 4950 -660 5200 -830 5480-1140 5720-1160 6090-1200 6450-1250 6860-1190	93
39 58	504 7280-1050 7710 -870 8160 -850 8790 -900 9460 -85010170 -80010860-1010	83
39 58	50511790-125012770-140013710-151014840-162016160-174017300-183018410-1900	51
39 58	50620220-205021950-217023450-228025000-237026630-246028140-254029880-2670	85
39 58	50731360-271032520-280033610-286034700-2920	9
39 58	521811117 1330 48-2650 1280 1920 1550 1960 1690 1980 1700 2030	93
39 58	522 1810 1730 1920 1580 2030 1560 2140 1650 2210 1290 2360 1080 2510 910	79
39 58	523 2530 920 2820 760 3110 490 3500 140 3690 -200 3980 -320 4480 -520	53
39 58	524 4850 -720 5230 -990 5670-1170 6090-1180 6560-1110 7080-1090 7780-1090	35
39 58	525 8290-1080 8830-1060 9410-1040 9980 -97010690 -89011290 -94012040-1090	
39 58		99 680 77
39 58	52612470-119013310-137014250-149015100-159016250-170017350-179018880-1920	77
39 58	52720820-208022020-217022850-222024140-231025380-239026740-246027880-2530 52829170-259030380-2650	4
		82
39 58	551811130 1100 43-2540 1700 2020 1800 1760 1940 1570 2140 1530	87

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(Continued)

(Sheet 1 of 61)

Table B1. (Continued)

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39 58 552 2190 1300 2500 960 2570 900 2700 810 2800 770 3120 580 3340 230
                                                                                        58
      553 3630 -40 4010 -120 4360 -210 4660 -360 4980 -600 5420 -940 5980-1090
                                                                                        39
      554 6410-1070 6900-1080 7500-1070 8140-1110 8700-1130 9220-1160 9880-1120
                                                                                        99
      55510520 -99011130 -89011710 -93012410-108013240-127013950-140014890-1540
                                                                                        70
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(Sheet 3 of 61)

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39 62	234 3590 -90 3860 -450 4010 -540 4250 -630 4420 -740 4530 -850 4720 -970	66
39 62	235 4930-1050 5300-1170 5760-1190 5940-1180 6130-1150 6320-1110 6550 -920	21
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39 62	252 2380 1020 2500 910 2660 790 2790 630 2990 400 3520 -70 3670 -170	14
39 62	253 3990 -490 4290 -710 4650 -940 4950-1040 5140-1110 5320-1150 5580-1170	99

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Table Bl. (Continued)

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39 62 254 6010-1120 6140-1100 6340 -950 6460 -770 6680 -590 6910 -580 7220 -640
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39 62 272 2000 1670 2060 1770 2100 1850 2160 1700 2230 1210 2340 1080 2500 910
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39 62 273 2890 560 3100 410 3550 10 3740 -240 3780 -320 4100 -460 4270 -660
39 62 274 4570 -840 4790 -960 5040-1090 5260-1130 5680-1170 5870-1150 6000-1070
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39 62 443 3380 80 3650 -170 3920 -370 4190 -510 4470 -690 4760 -760 5140 -810
                                                                                       91
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39 62 461811016 1700 44-2420
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39 62 462 2140 1740 2230 1250 2400 980 2940 500 3350 110 3830 -170 4170 -390
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39 62 463 4590 -540 5010 -720 5450 -780 5910 -830 6380 -900 6700 -940 7040 -960
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PROCESS AND PROCESSES STORY OF SECONDS

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SERVICE PROPERTY PROPERTY OF STREET, MATERIAL PROPERTY BOLLING PROPERTY PROPERTY OF STREET, ST

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Table Bl. (Continued)

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Table B1. (Continued)

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(Sheet 46 of 61)

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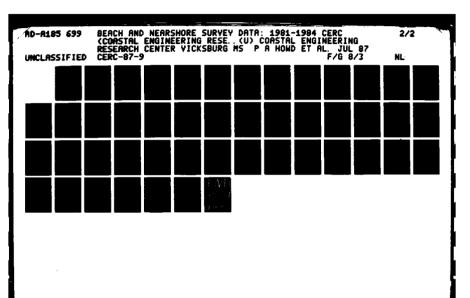
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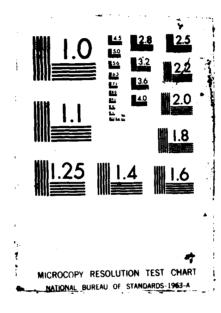
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(Sheet 58 of 61)

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Table Bl. (Continued)

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(Continued)

(Sheet 60 of 61)

Table Bl. (Concluded)

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•••••••••••••••••••••••••••••••••••••••	83
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CHARLESS CONTRACTOR ASSOCIATION CONTRACTOR

APPENDIX C: PROGRAM DATACHECK

The following program was written as an aid to the proper entry of the profile data into the user's computer system. The program was run on the correct data at the Field Research Facility and the proper checksum values added to the BPAS format file as explained in Appendix B. The data should be entered without the checksum values and then run through this program. Compare the checksum values with those given in Appendix B. The code was developed on a Control Data Corporation computer, but should be easily converted to any system running an implementation of FORTRAN 77.

```
PROGRAM DATCHK (INPUT, OUTPUT, TAPE7)
С
              AUTHOR: MS. REBECCA SAVAGE, WESCD-F
  THIS PROGRAM IS DESIGNED FOR THE DATA PROCESSER TO COMPARE COPIES
   OF DATA FILES TO MAKE SURE TRANSFERED COPIES ARE CORRECT.
   THE COPY CAN BE CHECKED AT EVERY LINE OR EVERY TEN LINES.
  THE PROGRAM READS FROM FORTRAN UNIT 7 AND WRITES TO UNIT 8
С
       INTEGER*2 ICARD(25), ITOT, LTOT, I, J, N, V, STOT
       CHARACTER*1 LINE(80), CARD(25)
С
       DATA ICARD/1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,
                  20,21,22,23,24,25/
       DATA CARD/'.',' ','-','0','1','2','3','4','5','6','7','8','9',
                 'G','H','D','E','O','M','R','C','V','A','S','B'/
  DATA IS READ IN LINE BY LINE
       N=1
       V=1
       STOT=0
   50 ITOT=0
       READ(7,100,END=99) LINE
  100 FORMAT(80A1)
С
  ASSIGN INTEGER VALUES TO CHARACTER DATA
С
  AND KEEP SUMS OF DATA BASED ON CHARACTER AND LOCATION IN LINE
       DO 10, I=1,80
          DO 20, J=1,25
           IF (LINE(I).EQ.CARD(J))THEN
             ITOT=ICARD(J)*I+ITOT
             GO TO 10
           END IF
   20
          CONTINUE
          WRITE (*,103) LINE(I),N,I
```

Processes and a second by the second
```
WRITE(8,103) LINE(1),N,I
          FORMAT('UNKNOWN CHARACTER ',Al,' IN LINE', 15,' AT COLUMN', 13)
  103
   10 CONTINUE
СС
C REDUCE THE SUMS TO A MANAGABLE LEVEL, KEEP A LINE SUM (LTOT)
C AND A SUM OF TEN LTOT VALUES (STOT). N COUNTS THE LINE NUMBER IN
C THE DATA FILE, V COUNTS THE TEN LINE INCREMENT FOR STOT.
C EACH LINE IS OUTPUT WITH ITS VALUE OF LTOT, EACH TENTH LINE
C ALSO INCLUDES STOT
      LTOT=MOD(ITOT, 100)
       STOT=LTOT+STOT
       N=N+1
       IF(V.EQ.10)THEN
         WRITE(8,101) LINE, LTOT, STOT
  101
         FORMAT(80A1,5X,215)
         V=1
         STOT=0
        ELSE
         WRITE (8,102) LINE, LTOT
  102
         FORMAT(80A1,5X,15)
         V = V + 1
       END IF
       GO TO 50
   99 STOP
       END
```

APPENDIX D: WAVE HEIGHTS AT PIER END, 1981-1984

This Appendix presents plots (Figures D1 to D4) of significant wave height at the pier end for each of the 4 years of this report, 1981-1984. The data from the pier-end Baylor wave staff have been combined with transformed data from the nearshore Waverider buoy to provide as complete a record as possible. It should be noted that the pier-end location becomes saturated with respect to wave height at approximately 2.8 m; thus, a value of 2.8 m may indicate that the significant wave height is greater farther offshore.

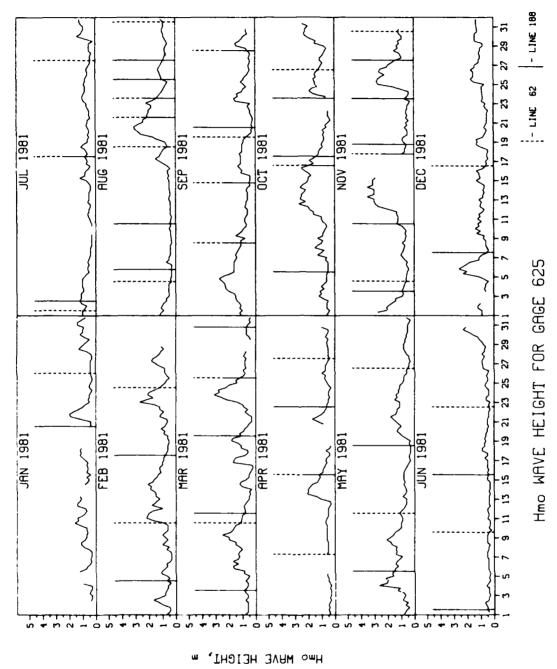


Figure D1. Wave height at pier end and times of surveys of lines 62 and 188, 1981

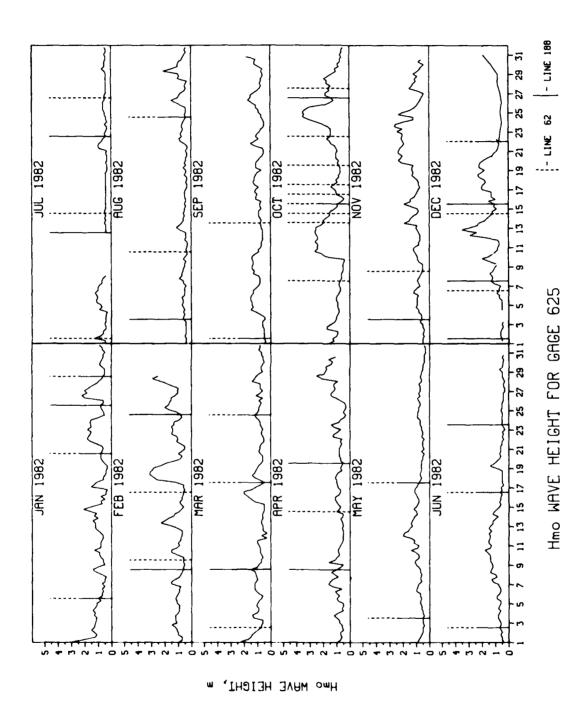
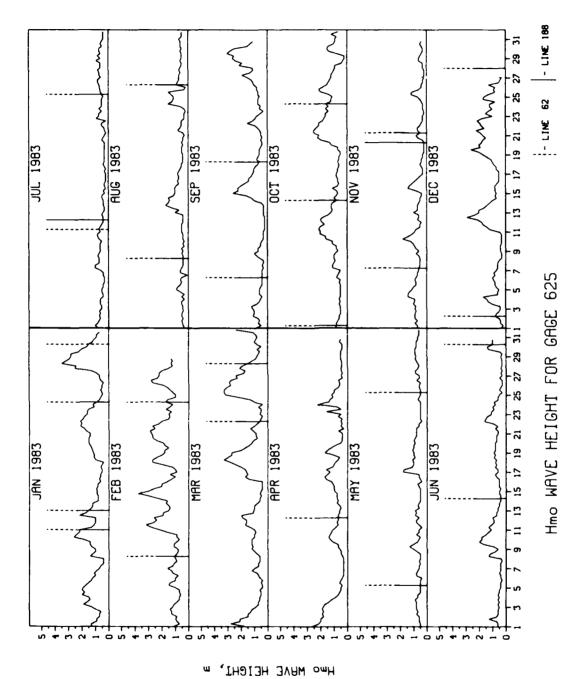


Figure D2. Wave height at pier end and times of surveys of lines 62 and 188, 1982



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Figure D3. Wave height at pier end and times of surveys of lines 62 and 188, 1983

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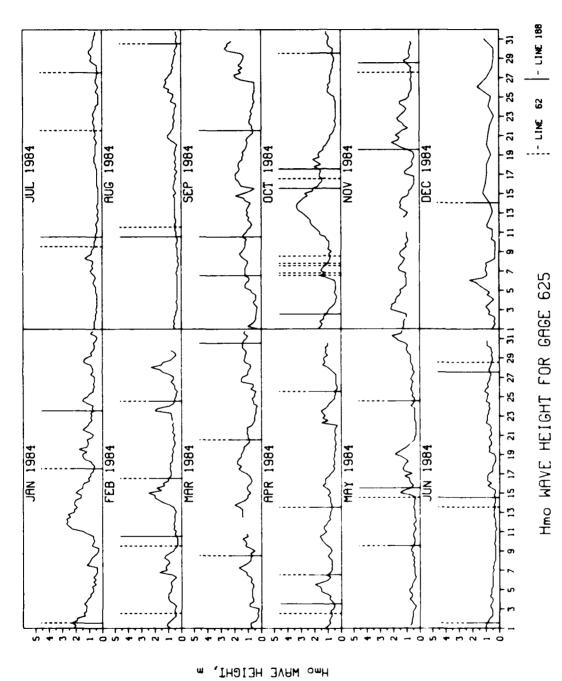


Figure D4. Wave height at pier end and times of surveys of lines 62 and 188, 1984

APPENDIX E: WAVE HEIGHT AND PEAK PERIOD, 1981-1984

Table El lists wave height and peak period for the 4 years covered by this report (1981-1984). The wave heights contained in the table are equivalent to those presented graphically in Appendix D. The periods are the period associated with the maximum energy peak in the wave spectrum calculated from a discrete Fourier transform of the record. Details of these calculations can be found in the main text.

Table El
Wave Data From 1981-1984

Message Resident Constituted Physicial Constituted

PLUS SEE PERCENTIAL SEED OF SECOND O

								
		JANUARY 1981		FEBRUARY 1981				
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)	
1	0						0.7	
_	1200						1.0	
							0.8	
	0						0.6	
	1200			-			0.7	
	100						0.6	
7	100			7			0.3	
8	115	5.0	0.9	8			0.5	
9	100	7.0	0.7	9			0.8	
10	105	4.0	0.7	10		10.3	0.6	
11	105	5.0	1.4	11	100	9.0	2.2	
12	105	4.0	0.8	11	700	9.0	2.1	
13	105	6.0	1.1				2.0	
14	1310	12.0	0.8	12	100	9.0	1.0	
15	105	10.0	0.5	13	100	7.0	1.2	
16	100	4.0	0.6	14	100	9.0	1.9	
17	1300	7.0	1.2	14	1300	12.0	2.1	
18	100	7.0	1.2	15	100	10.0	1.6	
20	1300	10.3	0.4	16	100	12.0	1.2	
21	100	9.1	0.4	17	100	10.0	0.9	
21	1900	8.0	2.0	18	100	9.0	0.6	
22	100	9.0	1.7	19	100	9.0	0.5	
23	100	9.0	0.5	20	100	7.0	0.8	
24	100	5.0	0.4	21	100	8.0	0.6	
25	100	3.0	0.4	22	100	9.0	0.9	
26	100	6.0	0.4	23	100	12.0	2.7	
27	100	10.8	0.4	23	700	14.0	2.2	
28	100	5.4	0.4	23	1905	16.0	2.1	
29	100	5.9	0.9	24	105	14.0	2.0	
30	100	5.0	1.2	25	100	14.0	0.8	
31	100	5.0	1.4	26	100	5.0	0.8	
				27	100	10.0	1.5	
	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 20 21 21 22 23 24 25 26 27 28 29 30	1 0 2 1200 3 0 4 0 5 1200 6 100 7 100 8 115 9 100 10 105 11 105 12 105 13 105 14 1310 15 105 16 100 17 1300 18 100 20 1300 21 100 21 1900 22 100 23 100 24 100 25 100 26 100 27 100 28 100 29 100 30 100	DAY TIME PERIOD (S) 1 0 10.0 2 1200 10.0 3 0 10.0 4 0 6.0 5 1200 6.0 6 100 6.0 7 100 12.0 8 115 5.0 9 100 7.0 10 105 4.0 11 105 5.0 12 105 4.0 13 105 6.0 14 1310 12.0 15 105 10.0 16 100 4.0 17 1300 7.0 20 1300 7.0 21 100 7.0 22 100 9.1 21 1900 8.0 22 100 9.0 23 100 9.0 24 100 5.0	DAY TIME PERIOD (S) HEIGHT (M) 1 0 10.0 1.1 2 1200 10.0 0.4 3 0 10.0 0.3 4 0 6.0 0.3 5 1200 6.0 1.2 6 100 6.0 0.6 7 100 12.0 0.3 8 115 5.0 0.9 9 100 7.0 0.7 10 105 4.0 0.7 11 105 5.0 1.4 12 105 4.0 0.8 13 105 6.0 1.1 14 1310 12.0 0.8 15 105 10.0 0.5 16 100 4.0 0.6 17 1300 7.0 1.2 18 100 7.0 1.2 20 1300 10.3 0.4	DAY TIME PERIOD (S) HEIGHT (M) DAY 1 0 10.0 1.1 1 2 1200 10.0 0.4 2 3 0 10.0 0.3 3 4 0 6.0 0.3 4 5 1200 6.0 1.2 5 6 100 6.0 0.6 6 7 100 12.0 0.3 7 8 115 5.0 0.9 8 9 100 7.0 0.7 9 10 105 4.0 0.7 10 11 105 5.0 1.4 11 12 105 4.0 0.8 11 13 105 6.0 1.1 11 14 1310 12.0 0.8 12 15 105 10.0 0.5 13 16 100 4.0 0.6 <td>DAY TIME PERIOD (S) HEIGHT (M) DAY TIME 1 0 10.0 1.1 1 100 2 1200 10.0 0.4 2 100 3 0 10.0 0.3 3 100 4 0 6.0 0.3 4 100 5 1200 6.0 1.2 5 100 6 100 6.0 0.6 6 100 7 100 12.0 0.3 7 100 8 115 5.0 0.9 8 100 9 100 7.0 0.7 9 100 10 105 4.0 0.7 10 700 11 105 4.0 0.8 11 700 12 105 4.0 0.8 11 700 13 105 6.0 1.1 11 12 100 1</td> <td>DAY TIME PERIOD (S) HEIGHT (M) DAY TIME PERIOD (S) 1 0 10.0 1.1 1 100 8.0 2 1200 10.0 0.4 2 100 7.0 3 0 10.0 0.3 3 100 10.0 4 0 6.0 0.3 4 100 9.0 5 1200 6.0 1.2 5 100 12.5 6 100 6.0 0.6 6 100 6.0 7 100 12.0 0.3 7 100 14.0 8 115 5.0 0.9 8 100 12.0 9 100 7.0 0.7 9 100 8.0 10 105 4.0 0.7 10 70 10.3 11 105 5.0 1.4 11 100 9.0 12 105 4.0</td>	DAY TIME PERIOD (S) HEIGHT (M) DAY TIME 1 0 10.0 1.1 1 100 2 1200 10.0 0.4 2 100 3 0 10.0 0.3 3 100 4 0 6.0 0.3 4 100 5 1200 6.0 1.2 5 100 6 100 6.0 0.6 6 100 7 100 12.0 0.3 7 100 8 115 5.0 0.9 8 100 9 100 7.0 0.7 9 100 10 105 4.0 0.7 10 700 11 105 4.0 0.8 11 700 12 105 4.0 0.8 11 700 13 105 6.0 1.1 11 12 100 1	DAY TIME PERIOD (S) HEIGHT (M) DAY TIME PERIOD (S) 1 0 10.0 1.1 1 100 8.0 2 1200 10.0 0.4 2 100 7.0 3 0 10.0 0.3 3 100 10.0 4 0 6.0 0.3 4 100 9.0 5 1200 6.0 1.2 5 100 12.5 6 100 6.0 0.6 6 100 6.0 7 100 12.0 0.3 7 100 14.0 8 115 5.0 0.9 8 100 12.0 9 100 7.0 0.7 9 100 8.0 10 105 4.0 0.7 10 70 10.3 11 105 5.0 1.4 11 100 9.0 12 105 4.0	

(Continued)

(Sheet 1 of 22)

Table El. (Continued)

				28	100	10.0	1.2
		MARCH 1981				APRIL 1981	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	12.0	0.8	1	100	8.0	0.4
2	100	10.0	0.6	2	100	6.0	0.5
3	115	10.0	0.6	3	100	8.0	0.3
4	100	5.0	0.6	4	100	14.0	0.3
5	100	7.0	0.5	5	100	6.0	0.6
6	100	16.0	1.7	7	700	9.0	0.6
7	100	10.0	1.2	8	100	9.0	0.5
8	100	12.0	1.2	9	1900	12.0	0.6
8	1900	14.0	2.0	10	100	11.0	0.6
9	100	14.0	2.0	11	100	10.0	0.6
9	700	14.0	2.5	12	100	10.0	0.5
10	100	14.0	1.6	13	100	5.0	1.1
11	815	12.0	1.0	13	1300	10.0	2.1
12	700	12.0	0.9	13	1900	11.0	2.0
13	100	14.0	0.5	14	100	11.0	2.0
14	100	12.0	0.3	15	100	10.0	1.2
15	100	6.0	0.7	16	100	7.0	0.9
16	100	9.0	0.3	17	100	8.5	0.7
17	100	6.0	1.6	18	100	6.4	0.7
18	110	12.0	0.6	20	1900	5.0	0.9
19	100	6.0	1.8	21	100	6.0	1.3
20	100	7.0	0.9	22	100	8.0	0.8
21	100	9.0	0.3	23	100	9.0	0.5
22	100	5.0	0.8	24	100	16.0	0.5
23	100	12.0	1.4	25	1300	13.7	0.8
23	700	14.0	2.2	26	100	5.1	1.0
23	1302	7.0	2.6	27	100	12.8	0.6
23	1900	8.0	3.1	28	100	12.1	0.5
24	100	10.0	2.7	29	100	3.8	0.6
24	700	12.0	2.8	30	100	7.0	0.6
24	1300	12.0	2.2				
24	1905	12.0	2.0				
25	117	12.0	1.4				
26	100	10.0	0.8				
27	100	10.0	0.8				
28	100	3.0	0.8				
29	1300	14.0	0.4				
30	100	14.8	0.7				
31	100	7.0	0.6				

Table El. (Continued)

		MAY 1981				JUNE 1981	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	5.0	0.8	1	700	8.0	0.4
2	100	3.0	0.7	2	100	4.0	0.6
3	100	5.0	0.7	3	100	8.0	0.3
4	100	10.0	2.7	4	100	9.0	0.6
4	700	9.0	2.1	5	705	9.0	0.3
4	1300	11.3	2.0	8	100	9.1	0.4
4	1900	12.0	2.2	7	100	8.0	0.5
5	100	10.0	1.6	8	100	8.0	0.4
6	105	10.0	1.2	9	100	9.0	0.5
7	100	8.0	0.9	10	100	9.0	0.4
8	115	5.0	1.3	11	105	8.0	0.5
8	1900	7.0	2.1	12	100	8.0	0.5
9	100	8.0	1.8	13	100	8.0	0.4
10	100	8.0	1.0	14	100	8.0	0.3
11	100	8.0	0.9	15	100	8.0	0.5
12	100	6.0	0.8	16	100	10.0	0.4
13	100	8.0	0.6	17	100	9.0	0.5
14	105	9.0	0.6	18	100	4.0	0.9
15	100	10.0	0.8	19	100	8.0	0.6
16	1300	8.0	0.5	20	100	9.0	0.5
17	100	8.0	0.3	21	710	8.0	0.5
18	100	7.0	0.3	22	100	6.0	0.4
19	100	8.0	0.3	23	100	6.0	0.3
20	100	6.0	1.3	24	100	3.0	0.4
21	700	5.0	1.6	25	100	5.0	0.6
22	100	8.0	1.3	26	700	10.7	0.4
23	100	10.0	1.1	27	700	4.7	0.9
24	100	10.0	1.2	28	100	5.7	0.9
25	100	10.0	0.9	29	100	5.3	0.8
26	100	9.0	0.6	30	100	10.5	1.6
27	100	9.0	0.4	30	1300	11.5	2.3
28	100	6.0	0.6	30	1900	7.7	2.1
29	100	8.0	0.8				
30	100	8.0	0.6				
31	100	7.0	0.5				
		JULY 1981				AUGUST 1981	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	10.6	1.0	1	100	6.0	1.2
2	100	7.9	0.7	2	100	7.0	1.0
3	100	8.2	1.1	3	100	7.0	0.5
4	100	7.6	1.0	4	100	9.1	0.5
5	700	7.4	0.7	5	100	9.0	0.3

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(Continued)

(Sheet 3 of 22)

Table El. (Continued)

6	100	8.4	0.6	6	100	9.0	0.3	
7	700	8.8	0.4	7	100	5.0	0.5	
8	100	8.7	0.4	8	100	10.0	0.4	
9	100	9.9	0.3	9	1300	7.0	0.4	
10	100	10.0	0.3	10	100	9.0	0.5	
11	1300	3.7	0.6	11	705	10.0	0.3	
12	100	9.6	0.5	12	700	10.0	0.4	
13	100	9.6	0.5	13	100	10.0	0.5	
14	100	9.1	0.4	14	700	12.0	0.5	
15	100	3.2	0.7	15	100	11.0	0.5	
16	100	6.1	0.7	16	100	10.5	0.6	
17	100	10.6	0.6	17	715	5.0	1.5	
18	100	4.4	0.7	18	700	6.0	0.9	
19	100	8.7	0.6	19	100	4.0	0.8	
20	100	8.3	0.5	19	2000	8.0	2.6	
21	100	6.4	0.6	20	200	9.0	2.8	
22	700	6.6	0.5	20	800	9.0	3.0	
23	100	8.4	0.7	20	1400	11.0	3.1	
24	100	8.3	0.9	20	2000	10.0	2.8	
25	100	6.8	0.9	21	200	11.0	2.4	
26	100	7.7	0.6	21	800	12.0	2.4	
27	100	8.2	0.5	21	1400	12.0	2.1	
28	100	6.6	0.4	21	2000	12.0	2.1	
29	100	2.1	0.5	22	200	12.0	2.0	
30	100	6.0	1.4	22	800	11.0	2.0	
31	100	4.0	0.9	23	200	12.0	2.2	
				24	710	11.0	1.0	
				25	700	12.0	0.6	
				26	700	6.0	1.2	
				27	700	8.0	1.0	
				28	700	9.0	0.7	
				29	100	8.0	0.7	
				30	100	6.0	0.9	
				31	100	7.0	0.9	
				▼-		. • •		

SEPTEMBER 1981

OCTOBER 1981

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	8.3	1.1	1	100	12.0	0.6
2	100	9.0	1.1	2	100	12.0	0.6
3	100	10.0	1.5	3	100	6.8	1.2
3	1300	12.0	2.0	4	100	6.0	1.0
3	1900	12.0	2.2	5	100	8.9	0.6
4	800	14.0	2.3	6	100	11.3	0.5
4	1400	12.0	2.5	7	100	3.6	0.6
4	2000	12.0	2.7	8	100	5.7	1.5
5	200	14.0	2.4	9	100	6.0	1.3
6	1300	11.9	1.6	10	100	6.0	0.7

(Continued)

(Sheet 4 of 22)

Table Ei. (Continued)

-	100	10 5	1.4	4.	100		• •	
7 8	100 700	12.5 11.4	1.4 1.1	11 12	100	5.0	1.0	
	100	10.8	0.8		100	6.0	1.9	
9		10.8		12	700	6.0	2.0	
10	100		0.9	12	1400	7.0	2.7	
11	100	12.5	0.8	12	2000	7.0	2.2	
12	100	11.4	0.6	13	200	8.0	2.6	
13	100	10.2	0.6	13	900	8.0	2.5	
14	100	11.8	0.7	13	1400	6.0	2.5	
15	100	12.0	0.4	13	2000	6.0	2.3	
16	200	14.0	1.0	14	100	8.1	2.2	
17	700	8.0	1.1	14	700	9.4	2.6	
18	100	12.0	1.0	14	1400	10.0	2.4	
19	100	11.0	0.9	14	2000	9.0	2.1	
20	100	7.0	0.3	15	200	10.0	2.0	
21	800	8.0	0.2	15	800	11.0	2.0	
22	100	11.0	0.4	15	1909	11.0	2.0	
23	100	9.0	0.4	16	109	12.0	2.3	
24	100	7.0	1.4	16	807	12.0	2.5	
25	100	6.0	0.9	17	200	11.0	1.9	
26	100	6.0	0.6	18	100	12.0	1.2	
27	100	10.0	0.5	19	700	10.0	0.8	
28	100	9.0	0.4	20	100	5.0	0.8	
29	100	6.0	1.4	21	100	9.1	0.5	
30	100	14.0	0.9	22	100	8.3	0.5	
				23	1400	7.0	0.7	
				24	100	5.0	1.6	
				25	100	5.0	1.5	
				26	100	7.0	1.5	
				27	100	10.0	1.0	
				28	100	6.7	0.9	
				29	100	4.0	0.8	
				30	200	9.0	2.2	
				30	700	8.0	2.3	
				30	1400	6.0	2.2	
				30	1935	7.0	2.2	
				31	200	7.0	2.0	
				31	800	9.0	2.4	

NOVEMBER 1981

DECEMBER 1981

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	900	12.0	2.7	1	100	7.0	0.9
1	1400	12.0	2.0	2	100	10.0	1.2
1	2000	12.0	2.1	3	1300	9.0	0.6
2	200	12.0	1.9	4	100	6.0	0.6
3	100	11.0	0.9	5	100	5.0	1.1
4	719	10.0	0.7	5	900	10.0	2.3
5	1405	7.0	0.5	5	1400	11.0	2.0

(Continued)

(Sheet 5 of 22)

Table El. (Continued)

6	805	6.0	0.6	5	2000	12.0	2.6
7	700	7.0	1.0	6	200	12.0	2.3
8	700	11.0	0.7	6	800	12.0	2.0
9	700	14.0	0.6	7	100	11.1	1.1
10	700	4.0	0.9	8	100	12.3	0.5
11	700	4.0	1.2	9	100	5.0	0.8
12	800	7.0	2.7	10	100	7.0	1.4
12	1400	8.0	2.9	11	100	7.1	1.2
12	2000	9.0	3.0	12	100	6.0	0.7
13	200	10.0	3.0	13	100	7.0	1.1
13	800	12.0	3.5	14	100	9.0	0.8
13	1400	10.0	3.0	15	100	9.0	1.3
14	200	14.0	3.0	16	100	10.9	1.3
14	800	12.0	3.5	17	100	9.9	0.6
14	1340	12.0	3.1	18	100	9.0	0.4
14	2000	11.0	3.1	19	100	6.0	1.2
15	200	12.0	3.1	20	100	6.0	0.6
15	700	12.0	2.9	21	100	6.0	0.5
17	1900	5.6	0.9	22	100	9.4	0.5
18	100	7.0	0.7	23	100	6.4	0.6
19	100	4.0	0.8	24	1300	5.3	0.9
20	100	3.5	0.5	25	100	5.1	0.7
21	100	4.0	0.6	26	200	6.0	1.5
22	100	4.0	0.6	27	100	6.0	1.4
23	100	4.0	0.4	28	100	8.0	1.0
24	100	12.0	0.4	29	100	9.7	0.8
25	100	8.0	2.7	30	100	5.7	1.4
25	800	9.0	2.8	31	700	4.7	1.3
25	1400	12.0	2.7				
25	1900	13.7	2.5				
26	100	13.1	2.2				
26	800	12.0	2.6				
26	1500	14.0	2.5				
26	2000	14.0	2.0				
27	200	17.0	1.9				
28	100	14.0	1.0				
29	100	6.0	1.3				
30	100	4.0	0.9				

JANUARY 1982

FEBRUARY 1982

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	10.0	2.9	1	100	8.0	0.9
1	700	11.0	2.1	2	100	5.0	1.0
2	100	10.0	1.3	3	100	7.0	1.1
3	1300	6.0	1.1	4	100	8.0	1.0
4	100	7.0	1.2	5	200	10.0	1.1
5	100	10 2	1 1		100	11 0	1.0

(Continued)

(Sheet 6 of 22)

Table El. (Continued)

6	100	12.6	0.7	7	100	5.0	1.5	
7	100	14.0	0.7	8	100	10.0	0.8	
8	900	6.0	1.3	9	100	11.0	0.5	
9	100	14.0	0.5	10	100	4.0	1.0	
10	100	6.0	0.9	11	100	10.0	0.9	
11	100	2.8	0.8	12	100	8.0	0.7	
12	100	4.4	0.6	13	100	6.0	1.5	
13	800	6.0	1.2	13	900	7.0	2.3	
14	200	10.0	1.3	13	1400	8.0	2.0	
14	1900	6.2	2.1	14	200	9.0	1.3	
15	100	7.5	1.5	15	100	10.0	0.6	
16	200	10.0	0.8	16	100	11.0	0.7	
17	200	6.0	1.5	17	100	7.0	0.6	
18	200	4.0	0.6	17	2000	10.0	2.6	
19	100	11.0	0.3	18	200	12.0	2.8	
20	100	6.0	0.8	18	800	11.0	3.1	
21	100	5.0	0.6	18	1400	11.0	3.1	
22	200	7.0	1.8	18	2000	12.0	2.9	
23	100	7.0	1.8	19	200	11.0	2.8	
24	100	10.6	1.5	19	200	11.0	2.8	
25	100	4.0	0.7	19	800	11.0	2.2	
26	100	8.4	0.6	20	100	11.0	0.8	
26	800	6.0	2.0	21	100	7.0	0.5	
26	1400	7.0	2.2	22	100	10.0	1.0	
27	200	7.0	2.0	23	200	9.0	1.4	
28	200	8.0	0.9	24	100	10.0	0.9	
29	100	12.0	0.5	25	200	6.0	1.7	
30	100	12.0	0.8	25	800	7.0	2.0	
31	100	5.0	0.5	26	200	6.0	1.5	
				27	200	11.0	1.0	
				27	2300	7.0	2.1	
				28	800	9.0	2.9	
				28	1400	10.0	2.5	
				29	2000	11.0	2.6	

POTATO PROPERTY RECEIVED STATES TANGED SERVICES

MARCH 1982	APRIL 19	Q 2
MAKCH 1302	AFRIL 19	04

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	200	11.0	2.2	1	100	9.0	0.9
2	903	10.0	0.9	2	100	10.0	0.7
3	100	8.0	0.6	3	100	10.0	0.8
4	200	6.0	1.0	4	100	6.0	0.9
5	705	8.0	0.9	5	100	10.0	0.5
6	100	3.0	0.9	6	200	5.0	1.0
7	200	10.0	1.2	7	100	7.0	1.6
8	800	6.0	1.2	8	700	6.0	1.4
9	100	8.0	0.9	9	100	5.0	0.5
10	730	5.0	0.8	10	100	7.0	0.8

(Continued)

(Sheet 7 of 22)

Table El. (Continued)

11	100	9.0	0.9	11	1300	8.0	0.5
12	100	11.0	0.7	12	100	11.0	0.5
13	100	12.0	0.6	13	100	4.0	0.5
14	100	11.0	0.6	14	100	7.0	0.5
15	100	11.0	0.5	15	100	6.0	0.7
16	900	8.0	2.0	16	100	5.0	1.1
16	1400	8.0	2.0	17	100	7.0	0.9
17	200	10.0	1.1	18	100	7.0	1.1
18	100	5.0	1.2	19	100	7.0	0.7
19	100	9.0	1.0	20	100	7.0	0.7
20	100	8.0	0.6	21	100	7.0	0.8
21	100	5.0	0.8	22	100	8.0	0.6
22	100	11.0	0.5	23	100	7.0	0.7
23	100	11.0	0.6	24	100	9.0	0.7
24	100	4.0	0.9	25	100	10.0	0.4
25	100	7.0	0.9	26	100	6.0	0.7
26	100	7.0	0.9	27	100	10.0	1.2
27	100	9.0	0.6	28	100	10.0	0.9
28	100	7.0	1.4	28	824	6.0	2.1
29	100	7.0	0.6	28	1400	7.0	2.5
30	100	9.0	0.5	29	205	9.0	1.8
31	100	9.0	0.7	30	200	8.0	1.3

MAY 1982 JUNE 1982

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	11.0	0.9	1	100	14.0	0.4
2	100	10.0	0.5	2	100	9.0	0.5
3	100	9.0	0.5	3	100	7.0	0.6
4	100	10.0	0.5	4	100	6.0	0.7
5	100	5.0	0.7	5	100	5.0	0.6
6	201	9.0	0.7	6	100	8.0	0.7
7	200	9.0	0.8	7	100	8.0	0.8
8	100	10.0	0.6	8	100	9.0	1.0
9	100	11.0	1.0	9	100	9.0	1.2
10	100	11.0	0.8	10	100	10.0	1.4
11	100	11.0	0.8	11	100	12.0	1.3
12	100	14.0	2.0	12	100	11.0	1.4
13	100	12.0	1.3	13	100	11.0	1.4
14	100	11.0	1.1	14	100	11.0	0.8
15	100	10.0	1.0	15	100	9.0	0.7
16	100	9.0	0.9	16	100	9.0	0.6
17	100	11.0	1.0	17	100	10.0	0.6
18	100	9.0	0.6	18	100	14.0	0.5
19	100	9.0	0.6	19	100	7.0	0.9
20	100	9.0	0.5	20	100	10.0	0.7
21	100	9.0	0.4	21	100	10.0	0.6
22	100	8.0	0.4	22	100	9.0	0.4

(Continued)

(Sheet 8 of 22)

Table El. (Continued)

-	-	•						
23	100	7.0	0.6	23	100	10.0	0.3	
24	100	7.0	0.7	24	100	8.0	0.5	
25	100	9.0	0.8	25	100	7.0	0.6	
26	100	9.0	0.8	26	100	11.0	0.4	
27	100	10.0	0.7	27	100	7.0	0.3	
28	100	9.0	0.6	28	100	8.0	0.3	
29	100	9.0	0.6	29	100	6.0	0.5	
30	100	9.0	0.4	30	700	8.0	0.4	
31	100	10.0	0.3					

JULY 1982

CONTRACTOR PROGRAM MARKAGA PROGRAM ORGANISMA (GARAGA MARKAGA NEW MARKAGA) PERENCES PROGRAM PERENCES PROGRAM PE

AUGUST 1982

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	10.0	0.4	1	100	14.0	0.4
2	100	5.0	0.6	2	100	12.0	0.4
3	100	6.0	0.5	3	100	12.0	0.4
4	100	5.0	0.4	4	100	11.0	0.5
5	100	6.0	0.8	5	100	10.0	0.7
6	100	7.0	1.1	6	100	8.0	0.5
7	100	6.0	0.9	7	100	9.0	0.4
8	100	9.0	0.4	8	105	6.0	0.7
12	1300	8.0	0.4	9	100	9.0	0.5
13	100	11.0	0.4	10	700	8.0	0.3
14	100	11.0	0.5	11	100	8.0	0.3
15	100	10.0	0.4	12	100	7.0	0.4
16	100	10.0	0.4	13	100	6.0	1.1
17	100	7.0	0.4	14	100	6.0	0.6
18	100	11.0	0.4	15	100	6.0	0.5
19	100	9.0	0.3	16	100	6.0	0.4
20	100	7.0	0.3	17	100	7.0	0.4
21	100	2.0	0.3	18	100	8.0	0.3
22	100	7.0	0.7	19	100	10.0	0.4
23	100	10.0	0.4	20	100	6.0	0.4
24	100	7.0	0.3	21	100	6.0	0.4
25	100	4.0	0.5	22	100	4.0	0.8
26	100	10.0	0.6	23	100	6.0	0.7
27	100	8.0	0.4	24	100	6.0	0.6
28	100	9.0	0.4	25	100	10.0	0.4
29	100	7.0	0.4	26	737	6.0	1.5
30	100	7.0	0.5	27	100	6.0	0.8
31	100	9.0	0.5	28	100	9.0	0.4
				29	100	6.0	1.0
				29	800	6.0	2.1
				30	100	7.0	1.0
				31	100	8.0	0.5

(Continued)

Table El. (Continued)

	SEPTEMBER 1982				OCTOBER 1982				
DAY 1	TIME 100	PERIOD (S)	HEIGHT (M)	DAY 1	TIME 100	PERIOD (S) 7.0	HEIGHT (M)		
2	100	6.0	0.5	2	100	10.0	0.9		
3	100	7.0	0.6	3	100	7.0	1.4		
4	100	9.0	0.8	4	100	9.0	0.9		
5	100	6.0	1.4	5	100	11.0	0.9		
6	700	6.0	1.3	6	100	14.0	0.9		
7	100	6.0	0.9	7	100	11.0	0.8		
8	100	4.0	0.9	8	100	8.0	0.6		
9	100	10.0	1.4	9	100	9.0	0.5		
10	100	11.0	1.4	10	100	6.0	1.8		
11	100	10.0	0.7	10	800	8.0	2.1		
12	100	8.0	0.6	10	1415	12.0	2.6		
13	100	6.0	0.7	10	2000	14.0	2.4		
14	100	6.0	0.8	11	200	14.0	2.4		
15	100	6.0	0.7	11	800	14.0	2.4		
16	100	10.0	1.1	11	1403	14.0	2.6		
17	100	11.0	1.1	11	2000	14.0	2.4		
18	100	10.0	1.2	12	200	14.0	2.4		
19	100	11.0	0.7	12	700	17.0	2.5		
20	710	6.0	0.8	12	1500	17.0	2.6		
21	100	8.0	0.5	12	2000	12.0	2.5		
22	100	6.0	1.2	13	200	14.0	2.5		
23	100	8.0	0.8	13	800	17.0	2.1		
24	100	11.0	0.5	13	1900	12.0	2.0		
25	100	9.0	0.9	14	822	14.0	1.5		
26	100	5.0	1.4	15	100	12.0	1.1		
27	100	8.0	1.3	16	100	11.0	0.4		
28	100	8.0	0.8	17	100	6.0	1.1		
29	100	9.0	0.6	18	100	14.0	1.0		
30	100	6.0	1.2	19	100	14.0	0.7		
				20	100	6.0	0.8		
				21	100	7.0	0.9		
				22	100	10.0	1.5		
				23	100	5.0	1.4		
				23	2000	6.0	2.1		
				24	200	7.0	2.6		
				24	800	8.0	3.1		
				24	1400	10.0	3.5		
				24	2000	12.0	3.4		
				25	200	14.0	3.5		
				25	800	14.0	3.3		
				25	1400	12.0	3.0		
				26	200	12.0	1.4		
				27	100	10.0	1.8		
				28	100	12.0	1.7		
				29	100	12.0	1.3		

(Continued)

(Sheet 10 of 22)

30	100	11.0	0.9
31	100	10.0	0.7

NOVEMBER 1982

THE PROPERTY OF THE PROPERTY OF THE PARTY OF

DECEMBER 1982

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	17.0	0.5	1	800	10.0	0.5
2	100	17.0	0.5	2	100	5.0	0.6
3	100	6.0	0.5	3	100	9.0	0.5
4	100	7.0	0.6	4	1300	10.0	0.5
5	100	6.0	0.9	5	100	10.0	0.5
6	100	8.0	0.8	6	100	12.0	0.7
7	100	7.0	0.7	7	100	11.0	0.6
8	100	9.0	0.7	8	100	6.0	1.2
9	700	11.0	0.5	9	100	6.0	1.0
10	100	5.0	0.9	9	2100	6.0	2.0
11	100	7.0	1.1	10	100	7.0	1.5
12	100	8.0	0.7	11	107	10.0	0.8
13	100	7.0	1.0	12	107	6.0	1.7
14	100	6.0	1.4	12	700	7.0	2.9
15	100	10.0	0.9	12	1400	11.0	2.4
16	100	6.0	1.4	12	2000	11.0	3.5
17	100	11.0	0.8	13	800	11.0	2.3
18	100	9.0	0.9	13	1400	12.0	2.2
19	100	7.0	1.3	14	1300	12.0	1.2
19	2000	8.0	2.1	15	100	12.0	0.9
20	200	8.0	2.3	16	100	7.0	1.0
20	800	10.0	2.1	17	100	6.0	2.0
20	1300	11.0	2.0	17	817	7.0	2.0
20	2000	12.0	2.3	18	100	6.0	1.8
21	200	12.0	2.3	18	800	7.0	2.2
21	800	12.0	2.2	18	1400	8.0	2.3
21	1400	12.0	2.0	18	2000	11.0	2.0
22	200	12.0	2.0	19	100	11.0	1.8
22	800	14.0	2.1	19	800	14.0	2.2
22	1500	14.0	2.0	19	1400	12.0	2.2
22	2000	14.0	2.0	19	2000	14.0	2.1
23	200	14.0	2.4	20	100	14.0	1.9
23	800	11.0	2.0	21	100	12.0	0.9
23	1400	14.0	2.6	22	700	17.0	0.9
23	2000	14.0	2.5	23	100	16.8	0.6
24	200	12.0	1.9	24	100	15.8	0.5
24	2000	7.0	2.3	25	100	14.0	0.6
25	100	6.0	2.0	26	100	15.3	0.5
26	100	6.0	0.8	27	100	7.8	0.6
27	100	10.0	0.4	28	100	5.7	0.8
28	100	7.0	1.2	29	100	6.3	0.8
29	100	6.0	1.2	30	100	4.9	1.3

(Continued)

(Sheet 11 of 22)

30 100 7.0 0.4 31 100 5.5 1.9

		JANUARY 1983			(FEBRUARY 1983	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	11.0	1.3	1	100	11.0	1.1
2	100	10.0	0.7	2	100	5.0	0.9
3	100	5.0	1.3	3	100	9.0	1.2
4	100	6.0	1.5	4	100	9.0	0.7
4	700	6.0	2.0	5	100	5.0	1.0
4	1900	7.0	2.0	6	100	8.0	1.0
5	100	9.0	1.9	7	100	9.0	1.6
6	100	7.0	1.2	8	100	11.0	1.0
7	100	9.0	0.7	9	100	12.0	0.8
8	100	9.0	0.4	10	100	6.0	0.7
9	100	4.0	1.0	11	100	6.0	2.2
10	100	7.0	1.9	11	700	8.0	2.8
10	700	10.0	2.6	11	1300	10.0	3.2
10	1300	10.0	2.4	11	1900	11.0	2.6
10	1900	10.0	2.2	12	100	12.0	2.4
11	100	10.0	2.1	12	700	12.0	2.6
12	100	10.0	1.0	13	100	12.0	1.5
12	1300	7.0	2.2	14	100	6.0	1.6
13	100	11.0	1.5	14	700	8.0	2.3
14	100	11.0	0.8	14	1300	10.0	3.0
15	100	14.0	0.9	14	1900	12.0	3.8
16	100	11.0	0.6	15	100	12.0	3.0
17	100	12.0	0.5	15	700	11.0	2.6
18	100	12.0	0.4	15	1300	12.0	2.0
19	1300	6.0	1.3	15	1900	12.0	2.0
20	100	8.0	1.5	16	100	11.0	1.6
21	100	6.0	1.4	17	100	12.0	0.9
21	1900	7.0	2.1	18	100	8.0	2.7
22	100	7.0	2.0	18	700	10.0	2.7
22	700	7.0	2.1	18	1300	11.0	2.4
23	100	9.0	1.6	18	1900	11.0	2.0
24	100	10.0	1.2	19	100	11.0	1.8
25	100	9.0	0.5	20	100	11.0	1.9
26	100	9.0	0.5	20	700	15.0	2.4
27	100	8.0	0.7	20	1300	15.0	2.7
27	1900	8.0	2.5	20	1900	16.0	2.7
28	100	9.0	2.4	21	100	15.0	2.8
28	700	11.0	3.5	21	700	13.0	2.9
28	1300	9.0	3.2	21	1300	15.0	2.5
28	1900	14.0	2.9	21	1900	14.0	2.7
29	100	12.0	2.8	22	100	14.0	2.2
29	700	12.0	2.8	22	700	13.0	2.0
29	1300	12.0	2.2	23	100	13.0	1.5

(Continued)

(Sheet 12 of 22)

Table El. (Continued)

29	1900	12.0	2.0	24	160	13.0	1.2	
30	100	12.0	1.6	25	100	12.0	1.0	
31	100	11.0	0.9	26	100	10.0	1.9	
				26	700	11.0	2.7	
				26	1300	12.0	2.8	
				26	1900	11.0	2.3	
				27	100	12.0	2.2	
				27	700	14.0	2.2	
				27	1300	12.0	2.0	
				28	100	12.0	1.2	
				=				

MARCH 1983

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APRIL 1983

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	8.0	1.8	1	100	7.0	2.6
1	700	11.0	2.8	1	700	11.0	2.2
1	1300	12.0	2.1	1	1300	11.0	2.0
1	1900	10.0	2.1	1	1900	10.0	2.0
2	100	11.0	1.5	2	100	12.0	1.8
3	100	11.0	0.9	3	100	8.0	1.8
4	100	10.0	0.6	4	100	11.0	0.9
5	100	12.0	0.4	5	100	9.0	0.5
6	100	10.0	0.6	6	100	9.0	0.4
7	100	7.0	1.0	7	100	14.0	0.3
8	100	8.0	0.6	8	100	9.0	0.3
9	100	9.0	1.2	9	100	8.0	0.6
10	100	10.0	1.2	10	100	11.0	1.3
11	100	9.0	1.0	11	100	13.0	1.1
12	100	10.0	1.6	12	100	10.0	0.7
12	1300	11.0	2.0	13	100	10.0	0.6
13	700	8.0	1.0	14	100	10.0	0.7
14	100	6.0	0.6	15	100	9.0	1.0
15	100	14.0	0.5	16	100	7.0	1.2
16	100	10.0	0.4	17	100	12.0	1.3
17	100	5.0	1.6	18	100	11.0	0.9
17	1300	8.0	2.0	19	100	6.0	1.7
17	1900	7.0	2.4	20	100	10.0	0.5
18	100	10.0	2.8	21	100	4.0	0.4
18	700	10.0	3.3	22	100	9.0	0.4
18	1300	11.0	3.0	23	100	10.0	0.5
18	1900	11.0	2.7	24	100	8.0	2.3
19	100	11.0	2.7	25	100	12.0	1.2
19	700	11.0	2.0	26	100	9.0	0.6
20	100	11.0	1.2	27	100	11.0	0.5
21	100	12.0	0.9	28	100	10.0	0.4
22	100	10.0	0.8	29	100	14.0	0.5
23	100	4.0	0.6	30	100	12.0	0.4
24	100	11.0	0.4				

(Continued)

(Sheet 13 of 22)

Table El. (Continued)

24	1900	6.0	2.2
25	100	8.0	3.2
25	700	11.0	3.3
25	1300	12.0	3.3
25	1900	14.0	3.1
26	100	14.0	2.8
26	700	15.0	2.9
26	1300	13.0	2.8
26	1900	13.0	2.3
27	100	13.0	2.4
27	1900	12.0	2.1
28	100	11.0	1.9
29	100	10.0	0.8
30	100	5.0	0.5
31	100	7.0	0.8
31	1900	6.0	2.4

MAY 1983

JUNE 1983

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	11.0	0.5	1	100	9.0	0.6
2	100	8.0	0.6	2	100	5.0	0.7
3	100	9.0	0.8	3	100	10.0	0.5
4	100	9.0	0.7	4	100	14.0	0.5
5	100	8.0	0.5	5	100	12.0	0.4
6	100	9.0	0.4	6	100	9.0	0.4
7	100	8.0	0.6	7	100	6.0	0.4
8	100	8.0	0.5	8	100	7.0	0.4
9	700	6.0	1.3	9	100	6.0	0.6
10	100	6.0	0.6	9	1900	7.0	2.0
11	100	9.0	0.6	10	100	7.0	1.8
12	100	10.0	0.8	11	100	8.0	1.1
13	100	5.0	0.9	12	100	9.0	0.9
14	100	8.0	0.5	13	100	9.0	0.6
15	100	10.0	0.5	14	100	8.0	0.4
16	100	12.0	0.4	15	100	9.0	0.5
17	100	7.0	1.8	16	100	6.0	0.5
18	100	9.0	1.0	17	100	9.0	0.6
19	100	9.0	1.0	18	100	8.0	0.8
20	100	8.0	0.9	19	100	9.0	0.9
21	100	8.0	0.8	20	100	9.0	0.8
22	100	9.0	0.6	21	100	9.0	0.6
23	100	9.0	0.5	22	100	4.0	0.9
24	100	7.0	0.5	23	100	6.0	1.1
25	100	8.0	0.5	24	100	9.0	0.8
26	100	17.0	0.6	25	100	9.0	0.5
27	100	8.0	0.6	26	100	11.0	0.3
28	100	14.0	0.6	27	100	11.0	0.3
29	100	11.0	0.8	28	100	11.0	0.3

(Continued)

30	100	10.0	0.8	29	100	4.0	0.4
31	100	9.0	0.7	30	100	7.0	1.4
		JULY 1983				AUGUST 1983	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	6.0	0.8	1	100	12.0	0.3
2	100	7.0	0.6	2	100	7.0	0.4
3	100	9.0	0.5	3	100	8.0	0.4
4	100	10.0	0.6	4	100	17.0	0.3
5	100	8.0	0.5	5	100	10.0	0.9
6	100	17.0	0.3	6	100	9.0	0.6
7	100	3.0	0.6	7	100	7.0	0.6
8	100	8.0	0.7	8	100	10.0	0.4
9	100	7.0	0.6	9	100	14.0	0.4
10	100	8.0	0.5	10	100	14.0	0.3
11	100	6.0	0.6	11	100	14.0	0.5
12	100	7.0	0.4	12	100	7.0	0.4
13	100	10.0	0.4	13	100	5.0	1.0
14	100	12.0	0.4	14	100	7.0	1.5
15	100	10.0	0.3	15	100	8.0	1.0
16	100	10.0	0.3	16	100	9.0	0.7
17	100	10.0	0.2	17	100	8.0	0.8
18	100	10.0	0.4	18	100	8.0	0.5
19	100	10.0	0.3	19	100	9.0	0.4
20	100	10.0	0.3	20	100	10.0	0.4
21	100	10.0	0.3	21	100	10.0	0.3
22	100	7.0	0.5	22	100	5.0	0.5
23	100	8.0	0.7	23	100	8.0	0.3
24	100	8.0	0.5	24	100	4.0	0.6
25	100	10.0	0.4	25	100	7.0	1.1
26	700	14.0	0.7	26	100	7.0	0.2
27	100	14.0	0.6	27	100	7.0	0.7
28	100	14.0	0.6	28	100	9.0	0.6
29	100	8.0	0.6	29	100	8.0	0.5
30	100	7.0	0.7	30	100	7.0	0.5
31	100	10.0	0.4	31	100	6.0	0.7
		SEPTEMBER 198	<u>)</u>			OCTOBER 1983	
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	4.0	0.9	1	100	11.0	0.9
2	100	8.0	0.7	2	100	10.0	0.6
3	100	5.0	1.1	3	100	10.0	0.5
4	100	12.0	0.5	4	100	14.0	0.6
5	100	10.0	0.6	5	100	14.0	0.5
6	100	14.0	0.4	6	100	14.0	0.5

(Continued)

(Sheet 15 of 22)

Table El. (Continued)

7	100	14.0	0.4	7	100	14.0	0.5
8	100	11.0	0.3	8	100	12.0	0.9
8	100	6.0	0.7	9	100	5.0	0.7
10	100	10.0	0.4	10	100	6.0	1.1
11	100	8.0	0.3	10	1900	7.0	2.0
12	100	14.0	0.2	11	100	9.0	2.0
13	100	14.0	0.3	11	700	9.0	2.1
14	100	4.0	0.5	11	1300	10.0	2.0
15	100	8.0	2.6	12	100	10.0	1.9
15	700	8.0	2.2	12	700	11.0	2.0
15	1300	7.0	2.2	13	100	11.0	1.2
15	1900	9.0	2.0	14	100	11.0	1.1
16	100	11.0	1.7	15	100	11.0	0.7
17	100	7.0	1.1	16	100	9.0	0.6
18	100	10.0	0.7	17	100	11.0	0.8
19	100	11.0	0.6	18	100	10.0	0.6
20	100	10.0	0.4	19	100	9.0	0.5
21	100	9.0	0.5	20	100	5.0	1.2
22	100	4.0	0.9	20	1300	6.0	2.0
23	100	6.0	0.8	20	1900	8.0	2.2
24	100	10.0	0.5	21	100	9.0	2.1
25	100	4.0	0.6	21	700	7.0	2.5
26	100	8.0	0.8	21	1300	10.0	2.5
27	100	9.0	1.5	21	1900	8.0	2.3
28	100	10.0	1.1	22	100	8.0	2.1
28	700	10.0	2.1	22	700	10.0	2.1
28	1900	9.0	2.4	23	100	12.0	1.6
29	100	11.0	2.6	24	100	12.0	1.4
29	700	11.0	2.5	25	100	14.0	1.1
29	1300	11.0	3.0	25	1300	6.0	2.0
29	1900	12.0	2.8	25	1900	7.0	2.1
30	100	9.0	2.5	26	100	10.0	1.8
				27	100	12.0	1.2
				28	100	6.0	0.9
				29	100	11.0	0.2
				30	100	8.0	1.5
				31	100	7.0	0.9

NOVEMBER 1983

DECEMBER 1983

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	8.0	0.7	1	100	7.0	0.3
2	100	7.0	0.9	2	100	14.0	0.5
3	100	7.0	0.9	3	100	3.0	0.4
4	100	11.0	0.9	4	100	6.0	1.4
5	100	12.0	1.1	5	100	8.0	0.5
6	100	14.0	0.9	6	100	8.0	0.9
7	100	12.0	0.6	7	100	12.0	0.7

(Continued)

(Sheet 16 of 22)

Table El. (Continued)

	·- ·- ·	- ·	Table El.	(Contin	ued)		
8	100	12.0	0.5	8	100	5.0	0.5
9	100 100	14.0	0.6	9	100 100	14.0	0.4
10	100	9.0 9.0	1.2 0.9	10 11	100	12.0 11.0	0.3 0.5
12	100	9.0	0.4	12	100	7.0	1.8
13	100	6.0	1.0	12	700	11.0	2.1
14	100	6.0	0.6	12	1300	9.0	2.9
15	100	5.0	0.4	12	1900	10.0	2.3
16	100	11.0	1.1	13	100	11.0	2.0
17	100	9.0	0.3	13	700	9.0	2.0
18	100	4.0	0.5	14	700	11.0	1.0
19	100	12.0	0.3	15 16	100	9.0	0.7
20 21	100 100	11.0 8.0	0.2 0.8	16 17	700 100	10.0 10.0	0.5 0.5
22	100	9.0	0.5	18	100	17.0	0.9
23	100	12.0	0.3	19	100	6.0	1.7
24	100	12.0	0.3	19	700	6.0	2.0
25	100	7.0	0.7	19	1300	7.0	2.6
26	100	10.0	0.4	20	100	9.0	2.0
27	100	10.0	0.2	21	100	7.0	1.7
28	100	12.0	0.3	21	1300	6.0	2.2
29	100	5.0	0.6	22	100	7.0	1.8
30	100	7.0	0.3	22	1300	10.0	2.1
				23 24	100 100	10.0 5.0	1.0 1.2
				25	100	7.0	1.6
				26	100	5.0	0.8
				27	100	9.0	0.3
				28	100	14.0	0.1
				29	100	9.0	0.5
				30	100	8.0	1.4
				31	100	7.0	1.7
		JANUARY 1984			1	FEBRUARY 1984	
		UNIOART 1904			•	FDWONK! 1904	
DA	Y TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1		10.0	2.1	1	100	6.0	0.9
1	700	11.0	2.0	2	100	11.0	0.6
1	1300	11.0	2.3	3	100	11.0	0.5
2	100	7.0	1.9	4	100	7.0	1.0
3	100	11.0	1.2	5	100	8.0	0.8
4	100	12.0	1.1	6	100	9.0	0.6
5	100 100	11.0 5.0	0.7 0.5	7 8	100 100	6.0 6.0	1.1 1.0
7	100	9.0	0.4	9	100	8.0	0.6
8	100	5.0	0.9	10	100	10.0	0.3
9	100	10.0	0.3	11	100	10.0	0.4
			(Cont	inued)			
						•	(Sheet 17
			I	E17			

JANUARY 1984 FEBRUARY 1984

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	10.0	2.1	1	100	6.0	0.9
1	700	11.0	2.0	2	100	11.0	0.6
1	1300	11.0	2.3	3	100	11.0	0.5
2	100	7.0	1.9	4	100	7.0	1.0
3	100	11.0	1.2	5	100	8.0	0.8
4	100	12.0	1.1	6	100	9.0	0.6
5	100	11.0	0.7	7	100	6.0	1.1
6	100	5.0	0.5	8	100	6.0	1.0
7	100	9.0	0.4	9	100	8.0	0.6
8	100	5.0	0.9	10	100	10.0	0.3
9	100	10.0	0.3	11	100	10.0	0.4

Table El. (Continued)

						<u></u>	
10	100	5.0	0.6	12	100	11.0	0.5
11	100	8.0	1.5	13	100	6.0	0.4
11	700	7.0	2.3	14	100	8.0	1.4
11	1300	9.0	2.5	14	1300	10.0	2.0
11	1900	10.0	2.7	14	1900	11.0	2.0
12	100	7.0	2.6	15	100	10.0	2.5
12	700	9.0	2.7	16	100	10.0	1.4
12	1300	9.0	2.4	17	100	9.0	0.8
12	1900	6.0	2.6	18	100	10.0	0.9
13	100	11.0	2.1	19	100	10.0	0.7
13	700	9.0	2.1	20	100	8.0	0.5
13	1900	12.0	2.1	21	100	10.0	0.5
14	100	12.0	2.1	22	100	11.0	0.7
14	700	11.0	2.0	23	700	3.0	0.8
15	100	12.0	2.0	23	1300	7.0	2.0
16	100	10.0	1.4	24	100	11.0	0.9
17	100	11.0	0.9	25	100	11.0	0.4
18	100	9.0	0.8	26	100	7.0	0.5
19	100	9.0	1.5	27	100	5.0	0.6
20	100	7.0	1.1	28	100	9.0	2.3
21	100	10.0	0.7	29	100	10.0	0.6
22	100	6.0	1.1				
23	100	4.0	0.8				
24	100	10.0	0.7				
25	100	9.0	1.1				
26	100	11.0	0.6				
27	100	11.0	0.6				
28	100	10.0	0.8				
29	100	6.0	1.2				
30	100	9.0	0.6				
31	100	9.0	0.4				

MARCH 1984

APRIL 1984

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	4.0	0.7	1	100	11.0	1.2
2	100	12.0	0.3	2	100	12.0	0.8
3	100	10.0	0.2	3	100	11.0	0.6
4	100	6.0	0.6	4	100	10.0	0.9
5	100	14.0	0.7	5	100	11.0	1.5
6	100	7.0	0.7	5	1300	12.0	2.0
7	100	6.0	1.4	6	100	12.0	1.0
8	100	12.0	0.8	7	100	9.0	0.7
9	100	7.0	0.5	8	100	11.0	0.7
10	100	10.0	1.2	9	100	11.0	0.7
12	1300	6.0	1.4	10	100	6.0	1.4
13	700	7.0	1.4	11	100	9.0	1.1
13	1900	10.0	2.0	12	100	7.0	1.0

(Continued)

(Sheet 18 of 22)

Table El. (Continued)

14	100	10.0	1.6	13	100	11.0	0.8
15	100	10.0	0.8	14	100	9.0	0.8
16	100	12.0	0.8	15	100	8.0	0.8
17	100	12.0	1.1	16	100	12.0	1.2
18	100	7.0	1.8	17	100	9.0	0.8
19	100	12.0	1.5	18	100	11.0	0.5
20	100	14.0	1.1	19	100	11.0	0.5
21	100	10.0	1.0	20	100	9.0	0.4
22	100	11.0	0.7	21	100	10.0	0.4
23	100	11.0	0.5	22	100	10.0	0.3
24	100	11.0	0.3	23	100	11.0	1.2
25	100	6.0	0.5	24	100	12.0	1.0
26	100	7.0	0.6	25	100	11.0	0.5
27	100	10.0	1.4	26	100	12.0	0.3
28	100	9.0	0.8	27	100	11.0	0.4
29	100	10.0	1.2	28	100	10.0	1.0
30	100	6.0	1.4	29	100	11.0	1.3
31	100	12.0	1.1	30	100	11.0	1.2

MAY :	1984	JUNE	1984

Accession research prepare

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	700	11.0	0.7	1	100	10.0	1.0
2	700	10.0	0.5	2	100	6.0	0.7
3	100	9.0	0.4	3	100	7.0	0.6
4	100	7.0	0.8	4	100	11.0	0.5
5	100	11.0	0.8	5	100	11.0	0.6
6	100	8.0	0.4	6	100	10.0	0.5
7	100	7.0	0.4	7	100	10.0	0.4
8	100	7.0	0.5	8	100	10.0	0.3
9	100	4.0	0.7	9	700	9.0	0.3
10	100	7.0	0.4	10	100	9.0	0.3
11	100	6.0	0.4	11	100	7.0	0.3
12	100	8.0	0.3	12	100	8.0	0.3
13	100	9.0	0.4	13	100	10.0	0.4
14	100	8.0	0.4	14	100	10.0	0.3
15	100	6.0	1.5	15	100	9.0	0.3
16	100	3.0	0.7	16	100	6.0	0.6
17	100	6.0	0.6	17	100	5.0	0.8
18	100	8.0	1.1	18	100	7.0	0.4
19	100	12.0	1.9	19	100	9.0	0.4
20	1300	11.0	0.4	20	100	9.0	0.6
21	100	9.0	0.3	21	100	9.0	0.6
22	100	10.0	0.3	22	100	7.0	0.7
23	700	10.0	0.4	23	100	5.0	0.9

(Continued)

(Sheet 19 of 22)

Table El. (Continued)

24	100	5.0	0.7	24	100	4.0	0.8	
25	100	7.0	0.6	25	100	7.0	0.9	
26	100	6.0	0.6	26	100	10.0	0.8	
27	100	7.0	0.6	27	100	9.0	0.7	
28	100	9.0	0.5	28	100	9.0	0.7	
29	100	6.0	0.7	29	100	11.0	0.5	
30	100	8.0	1.0	30	100	7.0	0.6	
31	100	6.0	1.8					
31	700	6.0	2.1					

JULY 1984

AUGUST 1984

DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)
1	100	9.0	0.6	1	100	8.0	0.5
2	100	8.0	0.5	2	100	10.0	0.5
3	100	9.0	0.5	3	100	10.0	0.3
4	100	8.0	0.4	4	100	8.0	0.3
5	100	9.0	0.5	5	100	14.0	0.3
6	100	6.0	0.6	6	100	9.0	0.3
7	100	7.0	0.9	7	100	9.0	0.3
8	100	8.0	0.7	8	100	9.0	0.3
9	100	8.0	0.8	9	100	9.0	0.3
10	100	7.0	0.6	10	100	7.0	0.3
11	100	10.0	0.4	11	100	5.0	0.4
12	100	9.0	0.4	12	100	8.0	0.4
13	100	9.0	0.3	13	100	8.0	0.5
14	100	12.0	0.3	14	1300	5.0	0.5
15	100	7.0	0.3	15	100	7.0	0.4
16	100	9.0	0.4	16	100	7.0	0.5
17	100	10.0	0.4	17	100	8.0	0.4
18	100	9.0	0.5	18	100	10.0	0.4
19	100	8.0	0.3	19	100	9.0	0.5
20	100	17.0	0.5	20	100	10.0	0.3
21	100	17.0	0.5	21	100	6.0	1.0
22	100	14.0	0.6	22	100	6.0	0.6
23	100	7.0	0.7	23	100	5.0	0.6
24	100	12.0	0.5	24	100	6.0	0.4
25	100	14.0	0.3	25	100	6.0	0.6
26	100	14.0	0.3	26	100	6.0	1.3
27	100	14.0	0.4	27	100	8.0	1.0
28	100	9.0	0.4	28	100	10.0	0.6
29	100	4.0	0.8	29	700	8.0	0.5
30	100	5.0	0.8	30	100	9.0	0.4
31	100	6.0	0.6	31	700	10.0	0.3

(Continued)

Table El. (Continued)

SEPTEMBER 1984				OCTOBER 1984				
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)	
1	100	8.0	0.3	1	100	10.0	1.7	
2	100	17.0	0.4	2	100	10.0	1.3	
3	700	17.0	0.3	3	100	9.0	0.9	
4	100	14.0	0.4	4	100	11.0	0.4	
5	100	5.0	0.8	5	100	11.0	0.4	
6	100	6.0	0.9	6	100	10.0	0.5	
7	100	6.0	1.2	7	100	6.0	1.5	
8	100	9.0	1.0	8	100	5.0	0.9	
9	100	6.0	1.4	9	100	9.0	0.7	
10	100	7.0	1.2	10	100	10.0	0.9	
11	100	8.0	1.1	11	100	12.0	1.6	
12	100	7.0	0.8	11	1300	9.0	2.0	
1.	100	5.0	1.0	11	1900	9.0	2.2	
14	100	6.0	0.8	12	100	10.0	2.3	
15	100	7.0	1.3	12	700	9.0	2.3	
16	100	6.0	1.6	12	1300	11.0	2.5	
17	100	7.0	1.9	12	1900	12.0	2.7	
18	100	8.0	1.7	13	100	12.0	2.9	
19	100	10.0	1.3	13	700	12.0	3.2	
20	700	9.0	1.0	13	1300	12.0	3.3	
21	100	11.0	0.8	13	1900	14.0	3.3	
22	100	9.0	0.7	14	100	14.0	3.2	
23	100	9.0	0.8	14	700	14.0	3.0	
24	100	12.0	0.6	14	1300	12.0	2.8	
25	100	11.0	0.6	14	1900	12.0	2.5	
26	100	10.0	0.5	15	100	12.0	2.7	
27	100	6.0	1.9	15	700	12.0	2.1	
27	700 100	7.0 9.0	2.0 1.4	15 16	1300	12.0	2.1	
28 29	100	10.0	1.3	17	100 100	12.0 12.0	1.6 1.6	
29	1900	7.0	2.5	17	1900	14.0	2.0	
30	100	9.0	2.7	18	100	17.0	1.5	
30	700	10.0	2.5	18	1300	14.0	2.1	
30	1300	11.0	2.5	19	100	17.0	1.7	
30	1900	10.0	2.2	20	100	14.0	1.1	
30	1300	10.0	2.2	21	100	11.0	0.8	
				22	100	10.0	0.4	
				23	100	11.0	0.4	
				24	100	9.0	0.4	
				25	100	7.0	0.5	
				26	100	11.0	0.9	
				27	100	11.0	0.8	
				28	100	10.0	0.6	
				29	100	10.0	0.5	
				30	100	10.0	0.6	
				31	100	9.0	0.9	
				••		***	•••	

(Continued)

(Sheet 21 of 22)

Table El. (Concluded)

NOVEMBER 1984					DECEMBER 1984				
DAY	TIME	PERIOD (S)	HEIGHT (M)	DAY	TIME	PERIOD (S)	HEIGHT (M)		
1	100	4.0	1.3	1	100	11.0	0.5		
2	100	7.0	1.1	2	100	10.0	0.3		
3	100	6.0	2.2	3	100	5.0	0.8		
3	700	7.0	2.1	4	100	7.0	0.4		
3	1300	7.0	2.1	5	1300	6.0	1.5		
4	100	8.0	1.8	6	100	9.0	2.2		
5	100	10.0	1.5	7	100	6.0	1.0		
6	700	10.0	1.0	8	100	5.0	0.6		
7	100	6.0	1.5	9	100	6.0	0.3		
8	100	6.0	1.2	10	100	10.0	0.3		
9	100	10.0	1.4	11	100	9.0	0.5		
10	100	10.0	0.9	12	100	5.0	0.8		
11	100	10.0	1.0	13	100	9.0	0.5		
12	1300	12.0	1.2	14	100	10.9	0.7		
13	100	12.0	0.9	15	100	12.3	1.2		
14	100	14.0	1.5	16	100	9.7	1.0		
15	100	7.0	0.8	17	100	9.8	0.9		
16	100	11.0	0.4	18	100	10.9	0.9		
17	100	5.0	1.1	19	100	9.8	0.6		
18	100	5.0	0.5	20	100	12.3	0.9		
19	100	5.0	0.4	21	100	12.3	0.8		
20	100	6.0	1.7	22	100	10.9	0.7		
20	700	6.0	2.1	23	100	9.8	0.4		
21	100	7.0	1.8	24	100	4.5	0.8		
22	100	4.0	1.2	25	100	9.8	0.6		
23	100	6.0	1.5	26	100	6.9	1.6		
24	100	4.0	1.2	27	100	8.8	0.9		
25	100	6.0	0.8	28	100	8.8	0.5		
26	100	8.0	0.6	29	100	10.9	0.4		
27	100	8.0	0.6	30	100	9.8	0.4		
28	100	9.0	0.6	31	100	6.4	1.1		
29	100	8.0	0.8						
30	100	11.0	0.7						

(Sheet 22 of 22)

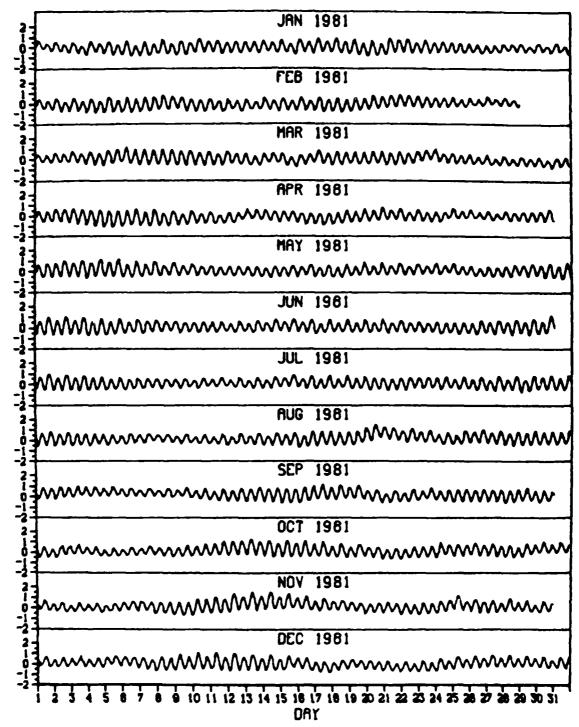
APPENDIX F: TIDE LEVELS AT PIER END, 1981-1984

This appendix contains plots of the observed tide levels at the end of the FRF pier. The data are collected by the National Oceanic and Atmospheric Administration/National Ocean Service (NOS) as part of their nationwide tide gaging program. Missing data have been interpolated by NOS. The tide gage, being located near the end of the pier, is occasionally within the surf zone. Thus, the tide data are influenced by setup, setdown, and storm surges, depending on the conditions at the time of the measurement.

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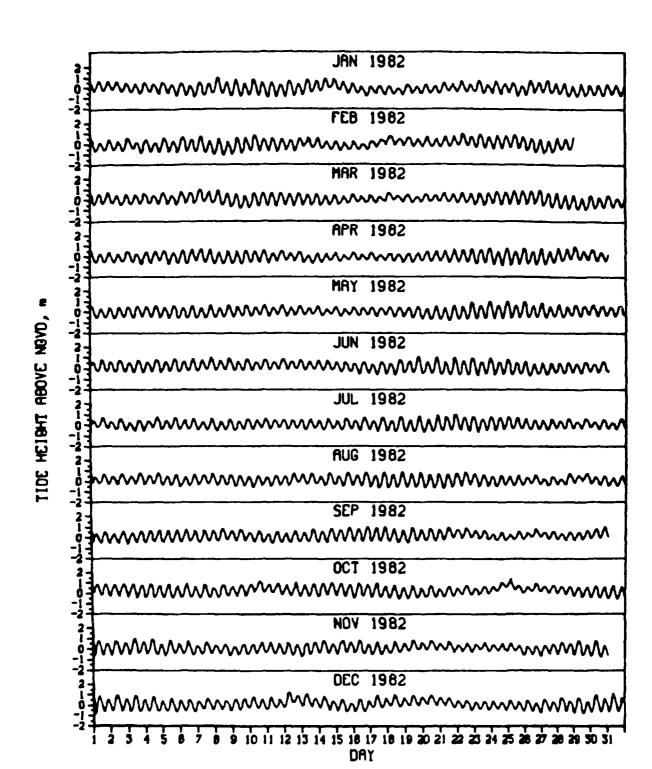
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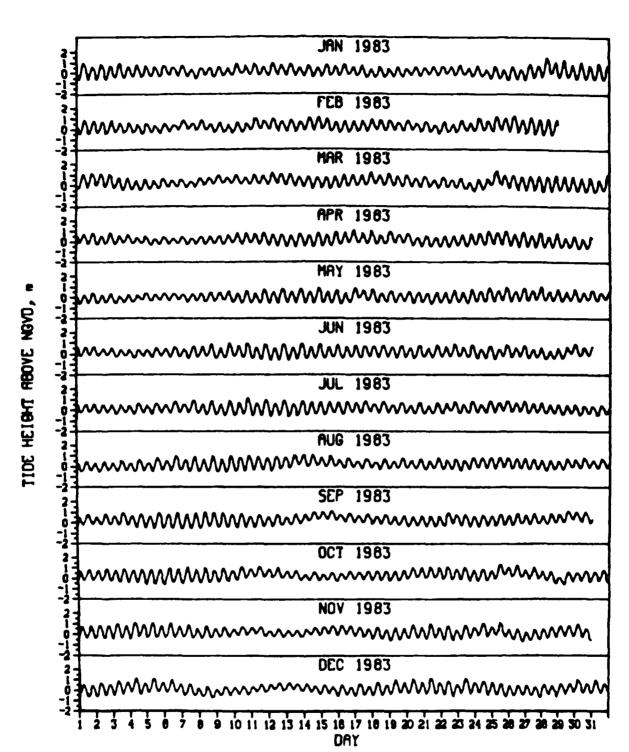
OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure Fl. Tide level record, 1981



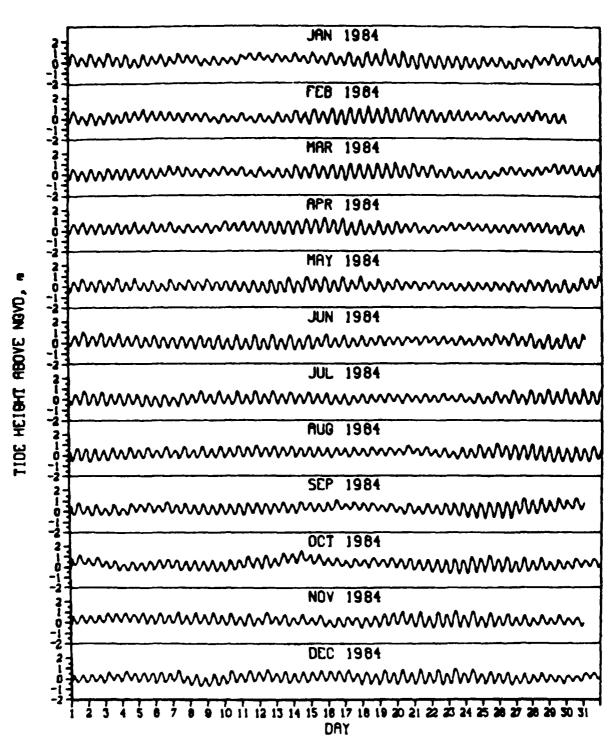
OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure F2. Tide level record, 1982



OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure F3. Tide level record, 1983



OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure F4. Tide level record, 1984

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